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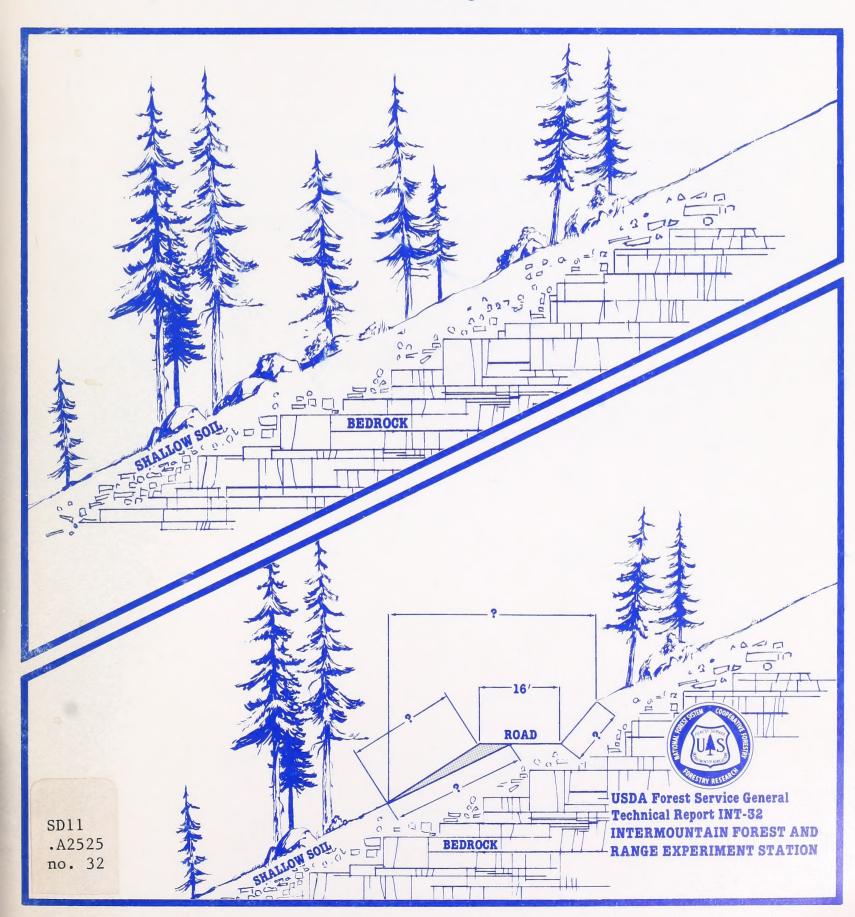
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TABLES OF GEOMETRY FOR LOW-STANDARD ROADS FOR WATERSHED MANAGEMENT CONSIDERATIONS, SLOPE STAKING, AND END AREAS

Walter F. Megahan





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ABSTRACT

Tables were developed to provide various dimensions for low-standard roads built with a "balanced" construction technique. The information is intended to provide a means of evaluating potential watershed impacts of road construction and of helping to plan for appropriate corrective actions. Additional dimensions are provided to assist in slope staking and for estimating excavation volumes. The information has application in both the road location and design phases of the road construction process. The tables are for use in situations where low road costs preclude detailed engineering design or where engineering talents are simply unavailable.

INTRODUCTION

Thousands of miles of roads are built each year on private, State, and Federal forest lands. Much of this annual construction consists of low-standard roads. These are low-cost roads receiving little or no engineering design either because the low road cost precludes more detailed engineering design or simply because no engineering talents are available.

Unfortunately, any type of road construction creates a variety of site disturbances that tend to accelerate erosion, which in turn may increase downstream sedimentation (Anderson 1954; Fredriksen 1970; Haupt and Kidd 1965). Low standard roads are often particularly troublesome because of such factors as poor location and design and lack of erosion control measures. Numerous other researchers have documented the occurrence of increased sedimentation following road construction, especially in steeper terrain (Megahan and Kidd 1972; Reinhart and others 1963; Rice and Wallis 1962). Such effects have become more important in recent years because of the enactment of Federal and State laws to regulate pollution by sediments from diffuse sources including roads.

Most of the potential impact is caused by accelerated on-site erosion including both surface and mass erosion (landslides). Some possible causal factors include:

- 1. Removal or reduction of protective cover;
- 2. Destruction or impairment of natural soil structure and fertility;
- 3. Decreased infiltration rates on parts of the road;
- 4. Concentration of generated or intercepted water;
- 5. Interception of subsurface flow levels by the road cut slope;
- 6. Decreased shear strength, increased shear stress on cut and fill slopes, or both;
- 7. Increased slope gradients on cut and fill slopes.

The last three factors are a direct result of the fact that road construction alters the geometry of the hill slope.

The primary purpose of the road geometry tables presented here is to provide a means of estimating the extent of alteration of hill slope geometry before construction. Use of the tables makes it possible to evaluate potential watershed impacts and to plan appropriate corrective actions. Such questions as:

- 1. How much area is disturbed by road construction?
- 2. What is the area of the rainfall intercepting surface?
- 3. What is the area of fill and cut slopes needing stabilization treatment?
- 4. Will channel encroachment occur?
- 5. How much area is available to buffer sediment flow into a stream channel?

These and other questions can be answered if various dimensions of the road prism are known.

Additional road prism dimensions are included for individuals concerned with slope staking and end areas. This information is included for three reasons:

- 1. Slope staking is needed to guide operators during construction so that the proper road prism dimensions are obtained;
- 2. Some of the dimensions needed for slope staking are already available from the calculations dealing with watershed management considerations;
- 3. A commonly used reference table for slope stakes and end areas for minor roads (USDA Forest Service and USDI Bureau of Land Management 1967) is out of print and is becoming generally unavailable.

ROAD PRISM DIMENSIONS CONSIDERED

The road prism dimensions pertinent to watershed management considerations are illustrated in figure 1. A description of the dimensions and some possible uses are:

- 1. SF = The slope distance from the grade daylight stake to the toe of the fill slope-
 - a. Provides a means of determining possible channel encroachment.
 - b. Defines the lower extremity of disturbed soil if channel encroachment does not occur; the distance from this point to the stream channel is the buffer strip that is available to trap eroded material. This information, coupled with guides for establishing the width of buffer strip (Ohlander 1976; Packer 1967; Trimble and Sartz 1957), provides a means of reducing sediment delivery to stream channels.
 - c. Indicates the hazard for "sliver" fills. A sliver fill is a fill constructed on a hill slope where the hill slope gradient approaches or exceeds the gradient of the road fill slope. When this happens no fill embankment can form; instead, the fill material flows down the hill in a long sliver. This tendency is apparent in the tables; as the hill slope gradients approach the fill slope gradient of 1-1/2:1 (66-2/3 percent), the values for SF increase rapidly indicating increasing probability of sliver fills. The tables do not exceed 66 percent because the values for SF go to infinity beyond this point.
- 2. SC = Slope distance from the grade daylight stake to the top of the cut slope--defines the limit of upslope disturbance and possible uphill encroachment (for example, into upslope landslide areas).
- 3. WH = Total width of disturbance projected to a horizontal plane--defines the total width of the rainfall intercepting surface.
- 4. WS = Total width of disturbance along the hill slope--defines the total width of the disturbed surface available for erosion.

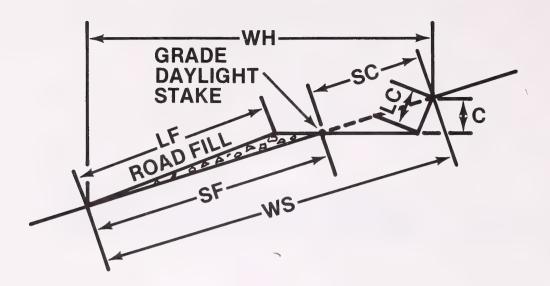


Figure 1.--Road prism dimensions for watershed management considerations.

- 5. LF = Length of the fill slope-
 - a. Useful for determining slope stabilization needs.
 - b. Often in combination with slope gradient is a useful parameter for estimating erosion by various procedures.
- 6. LC = Length of the cut slope--same uses as the length of fill slope.
- 7. C = Height of the cut, coupled with some knowledge of subsurface conditions (for example, soil depth or ground water depth), helps-
 - a. To indicate the potential for intercepting subsurface flow zones,
 - b. To red flag possible slope stability problems.

The road prism dimensions for slope staking and end areas are shown in figure 2. Descriptions and uses of the dimensions are:

- 1. SF = The slope distance from the grade daylight stake to the fill stake-determines the location of the fill stake.
- 2. SC = The slope distance from the grade daylight stake to the cut stake--determines the location of the cut stake.
- 3. C = The height of the cut--to be marked on the cut stake.
- 4. HC = The horizontal distance from the cut stake to the road centerline--to be marked on the cut stake.
- 5. F = The height of the fill--to be marked on the fill stake.
- 6. HF = The horizontal distance from the fill stake to the road centerline-to be marked on the fill stake.
- 7. A = End area, in square feet, of the cut section--to obtain cubic yardage per 100 feet of road length by multiplying average end area by 3.7.

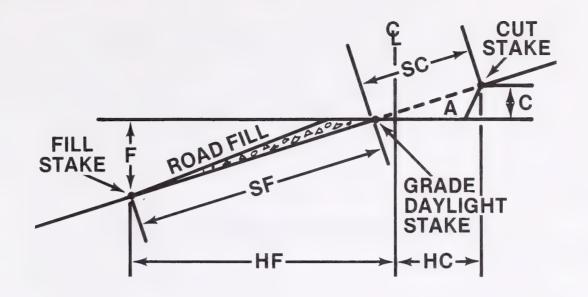


Figure 2. -- Road prism dimensions for slope stakes and end areas.

DEVELOPMENT OF THE TABLES

The road geometry tables in the appendix were developed using hill slope gradient (θ_s) , road width (W), and the gradient of the road cut (θ_c) and fill slopes (θ_f) as input variables (fig. 3).

Normally, these dimensions are known or can be closely estimated for a given situation. The most commonly used fill slope gradient on forest roads is 1.5 to 1; in the interest of economy, this is the only fill slope gradient given in the tables. Cut slope gradients of 1.5 to 1, 1.0 to 1, 0.75 to 1, 0.50 to 1, 0.25 to 1, 0.10 to 1, and vertical are presented. Hill slope gradients ranging from 10 to 66 percent are given in increments of 2 percent. Finally, road widths varying from 8 to 20 feet are given by 1-foot increments. The mathematical derivations are presented in the appendix so users can develop other combinations as needed. Calculations were programed in FORTRAN for a CDC 6600 computer; the program is available for use elsewhere.

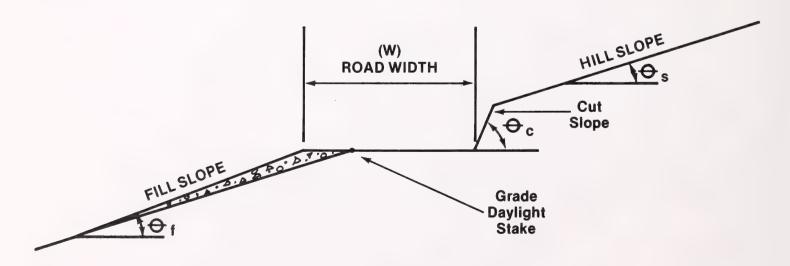


Figure 3. -- Dimensions required for road geometry tables.

The following assumptions were made in the development of the tables:

- 1. A "balanced" cut and fill is used for construction. Low-standard roads are commonly built by using balanced construction. This requires that the volume of material cut out of the hillside be equal to the volume of material used to construct the fill portion of the road. This type of construction is commensurate with low road standards because it minimizes excavation costs and because the low road standards permit fitting the road closely to the terrain (a requirement if balanced construction is to be used). Obviously, for economic reasons balanced construction can be just as desirable for roads built to higher standards. Unfortunately, this is not often possible except in areas of fairly uniform terrain. Elsewhere, horizontal and vertical irregularities prevent balanced construction and the use of these tables.
- 2. On the average, the fill section contains 15 percent less area than the cut section. This adjustment factor is necessary because many times variations in topography, type of materials, construction methods, or other situations prevent truly balanced construction. There can be more or less area in the fill slope than in the cut slope; however, there is generally less area in the fill slope because of problems during construction, such as downslope losses of materials. A shrinkage factor of 15 percent was assumed as an average value most applicable for low-standard roads. The adjustment factor is introduced in step 6 of the appendix as a value K; this value can be varied if necessary for other situations.
- 3. Slope gradients for cut slopes, fill slopes, and the hillside are relatively uniform. With proper construction, cut and fill slope gradients should be uniform. If the hillside gradient is relatively uniform, an average gradient for the section of slope in question may be used.
- 4. The road surface is horizontal. Many times roadbeds are insloped or outsloped to reduce erosion. However, the amount of slope is usually only a few percent and should cause only minor inaccuracies.
- 5. Cut and fill slope gradients are constructed as planned. Lack of compliance to planned cut and fill slope gradients can cause large errors in road prism dimensions. Obviously, this can only be prevented by careful adherence to plans during construction. Slope staking should help the operator meet specifications. It should be pointed out that fill slopes constructed by sidecasting (common on low-standard roads) may have a steeper gradient than 1.5 to 1 immediately after construction. Consequently the fill slope will not extend as far downslope as expected. However, over time, such an oversteepened fill slope tends to adjust to a 1.5 to 1 gradient and so meet the planned dimensions.

Except for situations where "balanced" construction is not used or where large irregularities in the hill slope gradients occur, minor deviations from the five assumptions above should cause only minor inaccuracies in road prism dimensions. The tables are only applicable to balanced construction and should only be used for this purpose. Where minor irregularities in the hill slope gradient occur, an average slope may be used without introducing large errors. However, as hill slope irregularities become large or as gradients approach 66 percent, large errors can be introduced. In this case, use good judgment to estimate what effect the break in hill slope gradient will have or use more intensive engineering design procedures to accurately cross-section the slope in question.

USE OF THE TABLES

Three factors must be known to use the tables: (1) road width, (2) cut slope gradient, and (3) hill slope gradient. A fourth factor, the fill slope gradient, is assumed to be 1.5 to 1 for all situations. A basic principle for minimizing watershed impacts from road construction is to minimize the amount of soil disturbance. This can be accomplished by selecting the narrowest road width possible and the steepest cut slope possible. However, selection must be tempered by user needs in the case of road width and by slope-stability requirements in the case of cut slope gradients. Generally, selection of road width is readily apparent depending on proposed road use; selection of cut slope gradients may require consultation with local expertise familiar with slope-stability problems in the area. The hill slope gradients are measured on site and used subject to the constraints discussed above.

Use of the tables also requires that a route location be available or assumed to serve as a reference point for measurements. This location is assumed to be a gradeline and is shown as the grade daylight stake on figures 1 and 2. Many times, the route location is established and the tables are used for slope staking and to help design stabilization needs. However, the tables are also helpful in selecting optimum route locations in areas where watershed management considerations are important. In this situation, a gradeline location is assumed and the road prism dimensions are determined. These are then compared to the actual conditions on the ground to appraise potential watershed impacts. Oftentimes, severe impacts become apparent that require a change in road location.

All dimensions in the tables are in feet except the end area, which is in square feet. The tables are suitable for roads that have additional width requirements for a berm or ditch. Simply add the additional horizontal distance caused by the berm or ditch to the basic road width and use the total width to enter the tables.

An example: watershed management considerations

As indicated above, the tables have a variety of potential uses for watershed management purposes. An example follows:

Given:

- 1. A 200-foot-long section of road located near an important fishing stream
- 2. Road width = 10 feet
- 3. Cut slope gradient = 1 to 1
- 4. Hill slope gradient = 50 percent
- 5. Slope distance from the grade daylight stake to the stream = 50 feet

Find: How can watershed impacts on the stream be minimized?

The first question would probably be "Will the road fill encroach on the stream?" Referring to the tables, we find that the slope distance from the grade daylight stake to the toe of the fill slope (SF on fig. 1) will be about 18 feet; so direct stream encroachment will not occur. However, this slope distance allows only 32 feet between the road fill and the stream, a distance that is judged to be inadequate after reference to guides for size of buffer area (Ohlander 1976; Packer 1967; Trimble and Sartz 1957). It is not practical to change the road location, but two alternatives are possible:

(1) Improve the efficiency of the buffer strip by adding materials to help store eroded material en route to the stream; or (2) control the erosion at the source by intensive

erosion-control measures. This particular stream is very valuable; so both courses of action are taken. The decision is made to augment sediment storage with the use of logging slash lopped and placed below the fill slope to assure close contact with the soil surface. On-site erosion control consists of mulching both cut and fill slopes and transplanting trees into the fill slope to help protect against mass erosion. Reference to the tables shows that the fill slope will be about 15 feet long (LF on fig. 1) and the cut slope will be about 9 feet long (LC on fig. 1). The total of these two figures times the length of road involved (200 feet in this case) indicates a need for mulching 4,800 square feet or about 0.1 acre. Planting trees at a 4- by 4-foot spacing on the 15- by 200-foot fill slope will require about 190 transplants.

An example: slope staking

Referring to figure 2, slope staking proceeds as follows using stations located at 100-foot intervals along the road. (If slope staking efforts must be curtailed, consider installing cut stakes only.)

- 1. Locate the position of the cut and fill stakes by determining the slope distance from the grade daylight stake to the slope stakes (SC for the cut stake and SF for the fill stake).
- 2. Determine the amount of vertical cut (C) or fill (F); and record on the cut and fill stakes, respectively.
- 3. Determine the horizontal distance from the slope stakes to the road centerline (HC for the cut stake and HF for the fill stake). Record on the cut and fill stakes, respectively.
- 4. Record the above dimensions along with the gradients of the cut and fill on the stakes. The cut and fill stakes for the hypothetical road dimensions given in the example above would appear as shown in figure 4.

As a point of interest, reference to the end area dimensions in the tables shows that the road section presented in the example on page 8 will require excavation of about 135 cubic yards of material.

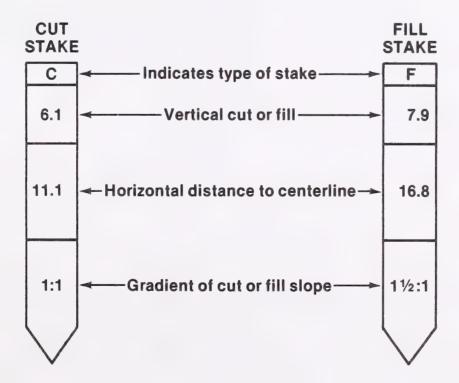


Figure 4. -- Dimensions for marking cut and fill stakes.

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APPENDIX

Procedure to calculate road prism geometry given the dimensions in figure 3:

W = Width of road (feet)

 θ_c = Angle of cut slope (degrees)

 θ_f = Angle of fill slope (degrees)

 θ_{s} = Angle of hill slope (degrees)

1. Calculate horizontal distance from gradeline to top of cut slope per foot of cut width (C_h) , where cut width is the distance from the grade daylight stake to the toe of the cut slope:

$$C_{h} = \frac{\text{Tan } \theta_{c}}{\text{Tan } \theta_{c} - \text{Tan } \theta_{s}}$$

2. Calculate slope distance from gradeline to top of cut slope per foot of cut width (C_s) :

$$C_s = \frac{C_h}{\cos \theta_s}$$

3. Calculate horizontal distance from gradeline to bottom of fill slope per foot of fill width (F_h) , where fill width is the distance from the grade daylight stake to the top of the fill slope:

$$F_{h} = \frac{\text{Tan } \theta_{f}}{\text{Tan } \theta_{f} - \text{Tan } \theta_{s}}$$

4. Calculate slope distance from gradeline to bottom of fill slope per foot of fill width (F_S) :

$$F_{s} = \frac{F_{h}}{\cos \theta_{s}}$$

5. Calculate the end area of the cut section for a unit cut width of 1 foot (A')

$$A' = 0.5 * C_s * Sin \theta_s$$

6. Assuming an equal area for the fill section times a correction factor (1+K) to account for shrinkage during construction, calculate the width of the fill corresponding to the unit width of the cut $(W_f^{'})$. An average 15 percent shrinkage loss was assumed for the tables; so a value of -0.15 was assigned to K in the development of these tables. Other K values can be applied as needed:

$$W_{f}$$
, = $\left[\frac{(1+K) * C_s}{F_s}\right]^{0.5}$ = $\left[\frac{(0.85) * C_s}{F_s}\right]^{0.5}$

7. Calculate the total cut width (B):

$$B = \frac{W}{1.0 + W_{f}}$$

8. Calculate the total fill width (W_f) :

$$W_f = W - B$$

9. Calculate the horizontal distance from the grade daylight stake to the road centerline (D):

$$D = B - 0.5 * W$$

10. Calculate the horizontal distance from the centerline to the cut stake (HC):

$$HC = C_h * B-D$$

11. Calculate the horizontal distance from the centerline to the fill stake (HF):

$$HF = F_h * W_f + D$$

12. Calculate slope distance from the gradeline to the toe of the fill (SF):

$$SF = F_s * W_f$$

13. Calculate slope distance from the gradeline to the top of the cut (SC):

$$SC = C_s * B$$

14. Calculate the total horizontal distance disturbed (WH):

$$WH = F_h * W_f + C_h * B$$

15. Calculate the total slope distance disturbed (WS):

$$WS = SF + SC$$

16. Calculate length of fill slope (LF):

$$LF = \frac{W_{f} * (F_{h}-1)}{\cos \theta_{f}}$$

17. Calculate length of cut slope (LC):

$$LC = \frac{B * (C_{h}-1)}{Cos \theta_{c}}$$

18. Calculate end area (A):

$$A = A' * B^2$$

19. Calculate cut height (C):

$$C = Sin \theta_S * SC$$

20. Calculate fill height (F):

$$F = Sin \theta_S * SF$$

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			6 .5	•	•	• •	1.	•	•	4 1.5]	_	•	3	• i	2.	2 6	, 0	2 3.1	8	60	m .	1 4°0	7	2 5.1	S OAD DIME	ROADFILL SF
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	3	1 00	ر م م	0	0	8	01 6	10	_ '	.2 10.		5 11	12	12.			4	4 0 1	16	1 17	3 19	20	.3 26.	8 31	_	4 82 	NO ES LO
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ROAD GEOMETRY DATA USING A 1.5 TO I FILL SLOPE

1 01 00	A	1.0	1.2	•	•	• •	1 .	- 6			3.7			6.4					7.6		. 1	10.0	0	5	13.4	un i	1	25.5		100 100 100 100 100 100 100 100 100 100
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	La.	4.	ທູ	1.	æ (1.0	1.2		1.5		1.9	•				3.2					5.6		•		10.1	• (90	53.5	E STAKIN	SF = SLOF C = CUT HC = HOR F = FILL AF = HOR
0 0 0 0 0 0 0 0 0 0 0	HC					4 4 • 0		•			4.8			5.0	•	•					5.7				6.3			7.5	ONS FOR SL	SC STAKE GRADE GRADE BAYLIGHT STAKE
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8 8 8 8 8 9	ΓC		9.			1.0			1.5	1.7	1.8			2.3		•	•				3.9				5.2	•		7.9	iα	PE FILL
	7	æ] • J	1.2	7.	9.8	2.1	-	2.7				4.1		5.1	•			7.9		•				0	•	6			O TOE FILL O TOP CUT STURB, HOR STURB, SLOP L SLOPE
8 9 9 1 1 1 1		R.9		•			10.5	- 4	•	11.7	12.1			\sim		S	5	9	17.7	œ	0		3.	9	0.	. 4		109.9	D MANAGEME	PE DIST. TO WIDTH DIST. WIDTH DIST. FILLIGHT OF CUT
	3		•	•	•	• •		-		•	11.6							15.3	16.1	17.0	•	6	0	2.	5	•	1 4	91.7	R WATERSHI	SF = SLO SC = SLO WH = TOT WS = TOT LF = LFN C = CUT
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AD WIDIN						N.0	1 .				•			7.6		•					12.4	•	15,3	~	20.1	24.1	0 0	43.4	AD DI	RADE WH-
0	SLOPE	10	12	14	91	18 20	22	24	92 9	28	36	32	34	36	38	40	42	77	94	48	50				58			0 4 4	1 1 1 1 1	

ROAD GEOMETRY DATA USING A 1.5 TO 1 FILL SLOPE

SLOPE 10 12 14 16 18 20 22 24 26 28 30		SC 86 90 90 90 90 90 90 90 90 90 90 90 90 90	I i	S	u -		Ç		L		
			1			L C	ر	QH.			A
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94	11.0	8.2	17.5		8.3	4.3		9.9	4.6	0	4.8
48			18.6	0							
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52	4		-	t i	12.1					14.1	
	9		\sim	9	4 •					10	
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62			39.8	6.	-			•	~	•	0
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9	110.1	•	105.		6				0	S.	2
	D DIMENS	IONS FOR	ATERSHED				DIMENSION	S FOR SLO	STAKIN	D END A	EA
STAY STAY	WH I I I I I I I I I I I I I I I I I I I	1 (3)		T. TO T. TO H DIST H DIST	0E 0P RB.	FILL +	2000	SC STAKE	SF = SLOPE SC = SLOPE C = CUT H HC = HOR.	DIST. DIST. EIGHT DIST. CU	
	SF_WS	_	C = LENGT C = CUT H	OF CUT	0	1	SF	GRADE DAYLIGHT STAKE	11111	DIST	STAKE T
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ROAD GEOMETRY DATA USING A 1.5 TO 1 FILL SLOPE

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9		•	0.0		7 F	1 . 1			0 0		•
	5.4	• •	10.7		0	. S	1.1	5.1	1.1	9.0	
22	5.6		11.0	11.3	1 .				1.2	5.8	2.6
70			11.4	11.8			1.4		1.4		
9				. 0					1.6		
80 0		6.3	12.3		&. €.1		1.7	7.0	1.7		
30			12.8	13.4			6 • T	* 1	•	6.0	7 0 1
32		•	13.4								
34	7.6	7.1			4 • 4		2.3			7.7	5.1
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æ «			15.4	16.5					•	•	
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54	7.		9								
99		13.4		3.	ď	6.6	6.5		0	٠. ص	ξ,
5.8	4.		3		21.8				12.1		19.
09	29.4	16.0	38.9	0 1			• [12,2	S i	9 1	5
		7.		5	34.2		4.6	6	20.1	4	9
94	52		. 4	76.0	54.5	15.4		14.9	30.1	64	33°3
	0	. 4	129.5	5.2			3	_	72.1	2	• 9
0 6 6 8 8	OAD DIMEN	STONS FOR	ATERSHED	MANAGEMENT	8 8 8 8 8 8 8	ROAD	DIMENSION	IS FOR SLOP	E STAKIN	END A	REAS
	STA A	1000	F = SLOPE C = SLOPE H = TOT.	DIST. TO	OE FILL OP CUT RB. HOR			i ≒≱\ıo	SF = 50	DIST. TO DIST. TO EIGHT	
	RONDER SE		OT ENGT	DTH DIST OF FILL OF CUT	URB. SLOPE SLOPF SLOPF	FILL	ROAD FILL SEASON	GRADE DAYLIGHT STAKE	HC = HOR. F = FILL HF = HOR.	DIST. CUT HEIGHT DIST. FIL	STAKE L STAKE
	\			-					1		

T0 1	V		• •											8.7			•	4.	17.3	C	. 4	ċ	300 000 000 000 000 000 000 000 000 000		900	571.8	A S	TOE FILL TOP CUT STAKE TO CL STAKE TO C - SQ. FT.
LOPE = 1.5	Ŧ				ນ 4 ຈ	1	• •			7.1	•		9.				12,5			7.	0	4.	7.65	• i	55.0	n an	D END ARE	DIST. TO
CUT SI	l <u>k</u>	υ «	7.	8	1.9		7	1.6		2.1	•		•	1 @ n m			5.7		. (9.1	•	13.4	17.1	• • •	; ;		E STAKING	SF = SLOPE SC = SLOPE C = CUT HE HC = HOR. [F = FILL H HF = HOR. [
	HC		•		ທ ທ ໝູ	1 (7.4	•	•		10.2	11.1	5		4	9	00	-	5.	31.9 41.5	• (, c	16.	VS FOR SLOP	C CUT SC STAKE GRADE DAYLIGHT STAKE
	ပ	N &	.7	6.	1.0		1.6					•	•				6.2		8.3			4.	18.6	• • •	• 4	274.7	DIMENSION	ROAD FILL TO SE
	٦٦	9.	1.3		1.9 2.1	1 4				4 •]		•		7.5	1 •	7.6			15.0		-	9	33.5	1 1	000	495.3		+u + +
	<u> </u>	α C	1.2	1.5	7.0	1		•		0				0.0			10.3		13.8	16.4	o*	• 4	30.9 41.49	: ; ,	ر د - د	• •	; ; ; ; ; ; ;	TOE FILL TOP CUT TURB. HOR. TURB. SLOPE SLOPE
	SM				11.1	12.2		•		15.2	9	•	o o	21.5	3	5	28.4	-	35.8	_	7.	57.3	71.1		34.	N C	MANAGEMENT	DIST. TO DIST. TO DIST. TO WIDTH DIS WIDTH DIS H OF FILL H OF CUT
	3	4°6	•	•	11.0	11.9			•	14.5	15.4	•	• a	20.02	1 -	3	25.8	œ	32.0	9	42.1	0	61.5		\$ 6	00	WATERSHED	SF = SLOPE SC = SLOPE WH = TOT. WS = TOT. LF = LENGT LC = LENGT C = CUT H
	၁ၭ				5.8 6.1	6.4			7.5	7.9	•	•	ر د	11.2	12.2		14.8		18.6	21.3			37°0 48.5	1	٠ ١	498.7	SI	1507
WIDTH = 8	SF				5 5 6 8	1			6°9		•	•	•	• •	11.2		13.6		17.2	6			34.1		5 ~	• •	AD DIME	SRADE WHAT I STAKE TO SEE SEE SEE SEE SEE SEE SEE SEE SEE SE
ROAD					2 S	22	24	56	28	30	32	3.4	0 C	07	42	77	94	\$	50		54	56	50 50 50 50 50 50 50 50 50 50 50 50 50 5	C7		99	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	

ROAD GEOMETRY DATA USING A 1.5 TO 1 FILL SLOPE

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SLOPE PERCENT	اسا	SC	I I I I I	SM	 			FC	 	¥	۵
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	•		6	•	1.1	9.1	9.1	9	9.1	•	•
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			•	•	•	o c				•	•
	5.7	• •	10.7	0		1.0	1.0	• •	1.1	•. •	• •
		1 .	10.9	11.2	2.3	1.1			1.3	1 •	1 .
	6.1		_	-		1.2			-		
			11.4			1.4	1.4		•		
33	• •	• •	• •	12.5	N 9 K K	1.5	1.5		• •	7.5	
				12.9	0.4	1.7	1.7				
		•	•	13.4							
		•	ه و			•					•
	3° C	0.9	13.5	14.4	7.4		7.0	Ն ո		0.0	
	•		1 .	0 }	0 1	Z • 3	. 1	• 1	0.0	• 1	• 1
42	6.5	6.3		15.7				4.5	3.7	10.0	
		0	2							•	•
	10.3		15.8	•	8.5		2.7			11,3	8.1
	•			10.4			•		•	•	
	. 1		:	. 1		. 1			• 1	• 1	• 1
	3		8	21.0			•				
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ر د د	0.00		0.4°0	α α ~ [[x		ري د د د		0.01	ر د و د د	0
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1	RADE WH-		= SLOPE = SLOPE = TOI	DIST. TO DIST. TO IDTH DIST	TOE FILL TOP CUT URB. HOR.			E CUT SC STAKE	B B B	DIST. DIST.	00E
	LOND FILL TERMS		S = T01. F = LENGT C = LENGT C = CUT H	DIH DIST OF FILL OF CUT GHT	URB. SLOPE SLOPE	STAKE	ROAD FILL TO SE	GRADE DAYLIGHT STAKE	HC = HOR. F = FILL HF = HOR. A = END A	DIST. CUI HEIGHT DIST. FILL REA OF CUT	STAKE STAKE
						,					

ROAD GEOMETRY DATA USING A 1.5 TO 1 FILL SLOPE

ROAD WIDTH = 9 FEET

CUT SLOPE = .10 TO 1

٩	1.		2.	m 9° 0		∾ (ຕໍ່ເ	n k	1 4	. 4	5	5	9	• 9		7.	ασ	9.6	10	11.	12.	13		1.71	• •	AREA	122 1 13
Ŧ				0.0	1.								0.6		10.1			13.2	1 .			19.9	• 1	28.6	82.1	A	PE DIST. PEIGHT DIST. CHEIGHT AREA OF
LE 1	ស្ម		Φ.	0 - 1		E .	4° I		2.0				3.0			•	•	5.8	1 4			10.2	• 1	16.0		PE STAKIN	SF = SLO SC = CUT HC = HOR HF = HOR
ΗÇ	•	4 4		4 4 0 0	1		•	•	• •	4.7				• [•		•	0 00		•			•	ທູນ	• •	VS FOR SLO	STAKE CUT C C
U	5.5		80.	0.1		1.1	E • 1	 	1.6	1.8				2.4		•		3.0	1 4			4.1	• 1	4 η Φυ	• •	S	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
۲c	5.	٥.	œ.	6.0		7.5	L • .		1.7	1.8			•	2.4	•	•) N	1 4			4.1	• 1	4 հ Ծ ഗ		1 <	-4-
F	6.	1.3	1.5	α ο ο						C • 7			•	6.1		•	•	10.4	1 4	13.5	•	α	• 1	0.80	· 6		TOE FILL TOP CUT TURB. HOR. TURB. SLOPE SLOPE
	6	• •	0	• •		11.3	• (יה יי		3	4.	14.7	5	9	9	. 0	20.1	1 -	9	5	28°6	•	39°5 52 4	0.40	ANAGEMEN	TO TO DIS DIS UILL
Z	•	• •		10.6	- 1		•	•	• •	1 .				14.3		2	•	18.0	16	C	2	24.8	•	33.5	• •	SHE	F = SLOP C = SLOP H = TOT• S = TOT• F = LENG C = LENG
SC	•	• •		ທ ທ ດ. ຕ	• I	•		•	• •				6.2			•	•	7.2	1 0			8.0	• 1	0.6	10.	IONS F	
SF							•			1 .				• (0		12.9	1 4	S	7.	4.02		30.4	1 m	AD DIME	SF WH
SLOPE PERCENT				0 0 0 0		22	500	0° c		32			38					50				85.4		52	99		1

ROAD GEOMETRY DATA USING A 1.5 TO 1 FILL SLOPE

ROAD WIDTH = 9 FEET

CUT SLOPE = .25 TO 1

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5	• •	• •			1.1	1.1	9 [1.1		
•9		11.2			1.2					
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14.6	•		ů.	12.1			•	•	14.6	
° α			t v					•	0 1	
2.0	•	26.0	•					•	• 🤇	0
2.55.2		9	4					13.0	24.0	16.5
1.7	9.	35.4	41.6		5.4	5.2	5.8	16.7	6	9
44.7	10.6	9.97	52.			•			0	21.4
98.8	11.7	92.3	110.		1.9		6.1	ν.	9	9
OAD DIMENSIO	NS FOR	ATERSHED I	ANAGEME		ROAN	DIMENSION	NS FOR SLO	PE STA	END AR	ا لعا أ
GRADE WH DAYLIGHT SC) o	SF = SLOPE SC = SLOPE WH = TOT W]	JIST. T	E FILL P CUT B. HOR.	-		SC STAKE	1 11 11 11	DIST. TO DIST. TO EIGHT	TOE FILL TOP CUT
ROAD SF WS		1 11 11 11	0F F 0F C 6HT	0PE 0PE 0PE	STAKE	ROAD FILTER	GRADE DAYLIGHT STAKE	F = FILL HF = HOR. A = END A	HFIGHT DIST. FILL REA OF CUT	STAKE - SQ.

ROAD GEOMETRY DATA USING A 1.5 TO 1 FILL SLOPE

ROAD GEOMETRY DATA USING A 1.5 TO 1 FILL SLOPE

										1 1 1 1 1 1 1 1
SF	35	HA	SM	LF	L C	U	HC	la.	اسا	۵
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5.7	7.51		11,5		1.3	100	5.3			
. 1	. 1	11.0	• 1			7°I	. 1	1.5	. 1	• 1
			12.3			1,3		1.3	. •	
		12.4	12.7			1.5				
7.1 7.5	6.6 6.8	13.2	13.7	ທຸຕ ທູດ	2.5	1.8	6.0	1.9	7.4	7 ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° °
		14.2						1 .	1	
8,3	7.3		15.6	4.8	2.9	2.4	6.3		8,5	6.1
		S								
6									6	
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24.5	12.8	32,3		22.2 27.5	& & • • • • •		0 0 0	12.3		
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54		59.	70.	0		8.8			48.5	
3.	18.9	Oi		123.0	3.		2	00 1	9	- 1
AD DIMEN	TONS F	WATERSHED	EME		ROAD	DIMENSION	SF	E STAKI	D END A	ш
GRADE WH GRADE STAKE STAKE FILE FILE ASS	307	SF = SLOPE SC = SLOPE WH = TOT. WS = TOT. LF = LENGT C = CUT H	DIST. TO DIST. TO MIDTH DIST WIDTH DIST H OF FILL H OF CUT	TOE FILL TOP CUT URB. HOR. URB. SLOPE SLOPE SLOPE	FILL	ROMO FILL TREES	SC STAKE SC STAKE GRADE GRADE GRADE GRADE STAKE	SF = SLOPE SC = SLOPE C = CUT H HC = HOR. F = FILL AF = HOR.	DIST, TO T DIST, TO T FEIGHT DIST, CUT S HEIGHT DIST, FILL	100 - 51

ROAD GEOMETRY DATA USING A 1.5 TO 1 FILL SLOPE

T0 1	۵									•	5.8				. 1	00	0		4 •	9	œ.	• 		9	2	58	AS OE FILL OP CUT TAKE TO O	50.
LOPE = 1.0	生	6. 6							7.5		8.2	0.3		° 0	. 1	11,0		. •		9	æ .	-	10	00	52	126.1	CUT FILL	EA OF
CUT SI	L.	n 0			1.0					•	2.5				•				• [•	•	•		2.		81.1	SF = SLOPE SC = SLOPE C = CUT H HC = HOR. F = FILL HF = HOR.	= END A
	£	0.0				5.9									. 1	8 8 6 9 6 9				10.5			13.7	5.	16.7	19.6	FOR SLOP	+ HC +
	U	ທູຈຸ	, &	6.	1.1	1 •			1.9						. 1								9.5	0	12.2	15.1	DI MENSION	¥
	C	2.6	1.1	1.3	1.5		2.2		2.7				•	4.						•			13.1	1 4	17.3	1,3	FILL F	
	LE	6.0	1.3	1.6	2.1	2.5								2.0	- 1					4.	7.	0	30.7	0		9 !	TOE FILL TOP CUT URB. HOR. URB. SLOPE SLOPE	
	SM		11.0		11.8	12.7								œ (19.0		6	5	co i	0	34.0	φ (1 %		174.6	MANAGEMENT DIST. TO DIST. TO MIDTH DIST WIDTH DIST H OF FILL H OF CUT	E 16H
	H	10.3			11.6	1 •	12.9	•		14.4	15.1			17.3	• 1		•	3	0	7.	6		3			145.7	WATERSHED SF = SLOPE SC = SLOPE WH = TOT WS = TOT LF = LENGI LC = LENGI	11
						1 .			7.1					φ (•		2	13.0	•	•	18.0	10	22.7	27.4	SIONS FOR	
WIDTH = 9	SF	50°0			5.8 6.1				7.3	7.7				° 6	10.4	11.2	13,1				20.0	23.0	33.1	42.9	2.	147.2	GRADE WH GRADE WHO WE WAS THE WA	\
ROAD	N FI	10			18 20				28					38									20		64			1

ROAD GEOMETRY DATA USING A 1.5 TO 1 FILL SLOPE

						1 1 1 1 1 1					
SLOPE ERCENT	SF	SC	3	S/3s	LF	٦٦	U	H	L	Ŧ	A
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14			11.4	11.5	1.4	•	Φ,		α <u>ο</u> (
				2.	1.6		0.1				
		•	å	2	1.9		1.2			•	•
			12.9	13.1	2.2	2.4	1.3	6.5	1.2		
22			13.4							. •	
54			14.1	14.5					1.6		
56				15.2							
28		8.4	15.5	9							
30	8.2		•	17.1	4.2	•	5.6	8.3	2.4	8.0	•
32	8.7	9.5		00							
75		c	α	0		•		- 1	4		
36	•	•	0	0				0	• 4		
38	10.7		0	~	•			0		0	
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	12.7		1 3	9	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	9.6		2		11.9	
		5	9	8	•						14.
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	17.1	∞	2	5				9		5.	8
20			9								
	22.3	24.0	6.04	1 5		20.0	1 -	1 -	10	16	1 10
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	∞	41.6	6	0	. 4	7.	0	5.	6	3	48.9
	0	54.6	0	5	46.7	0	oc 1	9	S	9	20
	72.6	78.7	I ~:	151.3	68.8			9	00	61.9	1
49	∞	9			24.	35				8	5
	517.3	561	00	078		7	0	68	84.		
		SIOI	iF	NAGEME		80	DIMENSION	S FOR SLO	PE STAKIN	END A	
	RADE WH	17/3	F = SLOP C = SLOP H = TOT.	DIST. T DIST. T WIDTH DI	OE FILL OP CUT RB. HOR			SC STAKE	SLOP SLOP CUT	DIST, TO DIST, TO IGHT	TOE FILL
	ROADER SE		OT. ENG	WIDT H OF H OF	RB LO	FILL	ROAD FILL FORESCE	GRADE	= HOR. = FILL = HOR.	DIST. CUT HEIGHT DIST. FIL	STAKE T
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• •		12.1	• •	.8 11.9 12.	.3 5.8 11.9 12.
2.5 1.3	0 0 0 0	12.4	.1 12.	.8 12.1 12.	.6 5.8 12.1 12.
2.9 1.4		12.7	.4	.9 12.4 1	.8 5.9 12.4 1
•		13.1		12.7	6.0 12.7
3.6 I.6 4.0 I.8		13.5	.3 13.	.2 13.3 13.	.4 6.1 13.0 13. .7 6.2 13.3 13.
	6 8 8			13.7 14.	.1 6.3 13.7 14.
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° 0		•	.5	.5 14.5 15.	6.5 14.5 15.
6.6 2.5		16.7	• •	15.5 16.	.8 15.5 16.
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2.9 3.		3	0.7 23.	.9 20.7 23.	.9 20.7 23.
4.7			2.2 25.	22.2 25.	7.1 8.1 22.2 25.
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4.		ທີ	.3 35.	30.3 35.0	6.3 9.0 30.3 35°.
1.3 5.	i i i	2	6.1 42.	.5 36.1 42.	3.0 9.5 36.1 42.
44.9 5.4 100.4 6.0	7	56.2 112.1	50	7.4 56. 3.6 112.	0.0 47.4 56. 1.0 93.6 112.
OAD (-	NAGEME	WATERSHED MANAGEM	SIONS FOR WATERSHED MANAGEM	AD DIMENSIONS FOR WATERSHED MANAGEM
E FILL CUT 3. HOR. STAKE FRILE FROADE	TOE TOP URB URB SLO	DIST. 1 DIST. 1 DIST. 1 WIDTH DI WIDTH DI H OF FILL	SF = SLOPE DIST. T SC = SLOPE DIST. T WH = TOT. WIDTH DI WS = TOT. WIDTH DI LF = LENGTH OF FILL C = LENGTH OF FILL	SF = SLOPE DIST. T SC = SLOPE DIST. T WH = TOT. WIDTH DI LF = LENGTH OF FIL	RADE WH SC = SLOPE DIST. I AYLIGHT SC = SLOPE DI

T0 1	۹	•		•	•	3.2		-			5.4			7.0				•	10.4	•		13.2	14.3		17.1	•	٠,	29.4	AS	OE FILL OP CUT TAKE TO CL. STAKE TO CL.
SLOPE = .10	Ŧ	ω. Θ. Α		9.	•		1	. (7.7			8.7		9.6	0		11.2			3.	14.6		17.5		22.1 25.8	•	e. ⊶ (91.2	D AR	DIST. TO
CUT SI	ᄕ	יי	•	0		1.3	1.4				2.2					•		4.6			4.9	7.3			11.4	•	٠	57.5	E STAKING	SF = SLOPE SC = SLOPE C = CUT HE HC = HOR. IF = FILL H A = END AF
	ΗĈ	5.1				5.1	5.1				5.2					5,3			5,3			5.4	5.4		ហ្វ	•		0 0 0	S FOR	C STAKE GRADE GRADE STAKE
	U	ง	•	ο σ		1.1	1.3	1.4	1.5	1.7	1.8	2.0													9°4	•	•	6.5	NOISN	ROAD FILL SE
	L C	2,		င့္		1.2					1.8					•			3.2		3.6				9.4	•		ຍູນ	iα	FILL
	ļ.	1.0				> m • • • •	2.6		3.2			4.5	n. O	5.5				A.3	9.5		11.6	3.	r,	7		•		103.6	1	TOE FTLL TOP CUT TURB. HOR. TURB. SLOPE SLOPE SLOPE
	SA		1101	11.4	0,7		12.6	-										8	6			. 4	9	00	31°8	• 1	າ ເ	116.1	NAGEME	DIST. TO DIST. TO DIST. TO DIST. TO MIDTH DIST. TO
	Z		1101	•	• •	12.0	18	- 6	8	3,	13.5	13.9	- 4				•	17.2	∞		0				27.5	• 1	•	6.96	ATERSHED	SF = SLOPE SC = SLOPE WH = TOT. WS = TOT. LF = LENGT C = CUT H
	SC			•		. w		-			6.4					7.0									ው ዕ ሆ	1	•	11.7	IONS F	
WIDTH = 10	S. F.	4.0	•	•				- 4			7.8					•			2			15.8	17.5	19.7	22.7		ם כ	104.3	OAD DIMEN	GRADE DAVIGHT STAKE LF FILL ROAD SF WS
ROAD	SLOPE PERCENT	10	21	1 4		20			56		30		34	36	38	0 7			46				54		5.0 5.0			99		

ROAD GEOMETRY DATA USING A 1.5 TO 1 FILL SLOPE

5.5 5.6 5.8 6.0 6.2 6.2 6.2 7.2 7.3 8.3 6.3 7.2 10.2 7.6	111	11.0 11.3 11.3 12.4 13.2 13.6 14.0	1.0						
55.6 56.2 56.2 56.2 56.2 56.2 56.2 57.2 56.2 56.2 57.2 56.2			1.2	9.	9.		5		
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66.0 6.2 6.4 6.4 6.7 7.0 7.9 9.1 7.9 9.1 7.0 6.0 6.0 6.0 7.0 9.1 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0			5.	Φ (Φ, (Φ.		
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7.2 6 7.5 6 7.9 6 8.3 6 8.1 7 9.1 7	mmm 1 4 4 mm 6			1.5	1.5		1.6		
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49.7 11.8	51.8	61.5	48.3		6.3		26.8	45.2	
9.8 13.	2	8	0	7.4	•	6.8	0	5.	
DIMENSIONS FOR WA	ED M	ANAGEMENT	9 6 8 8 8 8		DIMENSIONS	S FOR SLOPE	S	AND END AR	EAS
GRADE WH	= SLOPE = SLOPE	1ST. TO	FIL		المالية المالية	SC STAKE	SF = SLOPE D		TOE FIL
	= 101. = 101.	DTH D		STAKE F ROP	1	A		DIST. CUT	STAKE TO
-SF_WS	= LENGT = CUT H	OF CUT GHT	OPE	1		GRADE DAYLIGHT STAKE		ST	STAKE - SQ.

ROAN GEOMETRY DATA USING A 1.5 TO 1 FILL SLOPE

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RCENT	SF	၁၄	I	SA	الم	LC	U	HC	le.	HE	٥
	Ω.Ω.	5.7	11.1	11.2	0.1	9.	9.1	5.3	5,	. Ω . δ	1.5
	•	•	1104		O U	0	- a		α	•	•
				12.1	1.7	1.1	0	0.0	1.0	B. 0	
				2		1.2			1.1	. •	
		•	12.5		2.3	1.4	1.2			•	•
i 1					2.6	1.5	1.4	5.7	1.5	7.2	3.8
	7.1	6.5	13.2	13.6	3.0	1.7	1.5	5.8	1.7		
				4.		1.9	1.7		1.9		
	7.7			14.6		2°1	0°0	0.0	ا و د	ਦਾ ਹ © ਹ	
	• į	, . 1	. 1	T + C I	7.5	6.3	• 1	•	6.9	. 1	. !
				15.7	4.7						
	8°6	7.4	15.5	16.4	5.2	2.7	2.4	6.2	5.9	6,8	7.0
	6	•	•							6	
	•		16.7	,	4.9		•				
	0 1	•		18.8	7.1		. 1	. 1	3.9	0 1	. 1
	1.			6							
	2.		6	.0	8.8						
	13.1	0.6		22.1			3.8		5.5	13.2	11.9
	4		1:	23.6						14.2	
	2°		25.6	S.	12.5						•
1 2 2	17.1	10.1	4	27.3	14.3				7.9	16.9	15.6
	6	10.6	9	6	9	5.6				œ	17.1
		11.1		2.				7.7	10.6	6.02	œ
	5.			9	å					e.	21.0
0		12.4	36.4	42.5			6.4	0 1	15.5	28.3	
2	38.2	13.2		51.3	iœ	7.8		8.5	20.1	5.	26.8
				8			7.7			8	
	.3	16.1	4	4	C				9	05.	6
1	OAD DIMEN	101	ATFRSHED		8 8 8 8 8 8		IMENSION	S FOR SLO	1 <	D END AR	į lui
1	GRADE DAYLIGHT	100	S = SLO	DIST.	THE C			2	1	DIST. TO	TOP CUT
	ROADERT SE		ENG ENG	OF FIL	STURB. SLOPE L SLOPE SLOPE	FILL F RO	ROAD FILL TO A SE	GRADE DAYLIGHT	= HOR. = FILL = HOR.	DIST. CUT HEIGHT DIST. FILL	STAKE TO STAKE TO
-	\		TIC T	TUCT		1		STAKE		100	1

ROAD GEOMETRY DATA USING A 1.5 TO 1 FILL SLOPE

SLOPF	Ş	SC	I	SM	L	٦٦	U	HC	L	H L	Ø
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16			12.2	5			1.0				
				2	2.0		1.1				
	9.9	• (12.9	13.2	2•3	1.6	1.3		1.3		
		•	•	•		•			1.5		
		6.9	13.7	4 •					•		
				• 4					•		
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32			15.8	9					•		
34			•	7.	5.4			7.0			
	6			æ					•	0	•
	10.4	7°6	17.9	19.1					•		
	-	•		• 1			. 1		•	⊣ i	6.6
	-		6	21.3						•	
	2	•	0	2 °						2	
46	13.8	10.3		24.1	10.4	5.4		•	ທຸ		
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					C			6	11.4	e. ⊘i i	-
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62	2.	1 9	1 6			10.9	8.7	i -	22.2	38,2	32.6
	0	8	66.2	8	Œ				5	٠ س	6
				8	8		•	3.	S I	00	-
	AD DIMEN	210	ATFRSHED	i W		ROAD	DIMENSION	S FOR SLO	PE S	AND END A	الناأ
1	\$ 05 d S	1 557	= SLOPE = SLOPE = TOT•	105-	OE FILL OP CUT RB. HOR.	1		C CUT SC STAKE	= SLOP = SLOP = CUT	DIST. DIST.	TOE FIL
	Rohole SF WS		S = TOT. F = LENGT C = LENGT C = CUT H	WIDTH DI H OF FIL H OF CUT EIGHT	RB. SLO LOPE LOPE	FILL STAKE	ROAD FILL STATE	GRADE DAYLIGHT STAKE	HC = HCK. F = FILL HF = HOR.	A H H	STAKE TO
1						-		4 3 1			

ROAD GEOMETRY DATA USING A 1.5 TO 1 FILL SLOPE

1	040	WIDTH = 10	FEET							5 100	SLOPE = 1.0	101
Second S	SLOPF	S				- L		Ü	HC			۷
\$ 6.0 11.0 1		•			•	1.0	oc.			9.		•
Color Colo		•	•	•		1.2	1.0	. 7		· 7	•	
## 12.5 12.5			•	•	•	•	2.1	ĵ.		oc c	•	•
10 10 10 10 10 10 10 10		•	•	, c	2	•			•	0.	•	
7.0 7.1 13.8 14.7 2.7 2.2 11.5 6.5 11.5 7.3 4.1 4.6 5.1 1.7 7.4 4.6 5.1 1.7 7.6 4.4 5.1 1.7 7.6 4.4 5.1 1.7 7.6 14.8 15.3 3.5 2.4 7.4 2.5 1.9 1.9 7.9 5.8 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0			• •	3.	າ ຕ	• •					• •	
## 774 7.3 14.3 14.7 3.1 2.4 11.7 6.7 1.9 7.9 5.5 ## 8.5 15.4 16.0 3.9 3.7 2.1 7.1 2.2 8.3 7.9 5.5 ## 8.5 15.4 16.0 3.9 3.7 2.4 7.4 2.5 8.3 7.9 5.5 ## 8.5 15.4 16.0 3.9 3.7 2.4 7.4 2.5 8.3 8.5 ## 8.5 15.7 17.5 18.5 5.5 4.1 2.4 7.4 2.5 8.5 ## 8.5 15.7 17.5 18.5 18.5 18.5 18.5 18.5 18.5 ## 8.5 18.7 17.5 18.5 18.5 18.5 18.5 18.5 ## 8.5 18.7 18.5 18.5 18.5 18.5 18.5 18.5 ## 8.5 18.7 18.5 18.5 18.5 18.5 18.5 ## 8.5 18.7 18.5 18.5 18.5 18.5 18.5 ## 8.5 18.7 18.5 18.5 18.5 18.5 ## 8.5 18.7 18.5 18.5 18.5 18.5 ## 8.5 18.7 18.5 18.5 18.5 ## 8.5 18.7 18.5 18.5 18.5 ## 8.5 18.7 18.5 18.5 ## 8.5 18.7 18.5 18.5 ## 8.5 18.7 18.5 ## 8.5 18.7 18.5 ## 8.5 18.7 18.5 ## 8.5 18.7 18.5 ## 8.5 18.5 18.5 ## 8.5 18.5 18.5 ## 8.5 18.5 18.5 ## 8.5 18.5	22	1 •	1 .	1			1 .	1.5	1 .		1 4	
1.0	54											
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22.3 15.5 33.2 37.8 19.1 10.4 7.4 12.4 10.6 20.9 22.1 10.6 33.2 37.8 19.1 10.4 7.4 12.4 10.6 20.9 22.1 10.6 20.9 22.1 10.6 33.2 33.2 37.8 19.1 10.4 7.4 12.4 10.6 20.9 22.1 10.6 20.9 22.1 10.6 30.9 10.6 20.9 22.1 10.6 30.9 10.6 20.9 22.1 10.6 30.9 10.6 20.9 22.1 10.6 10.6 20.9 22.1 10.6 10.6 20.9 22.1 10.6 10.6 20.9 22.1 10.6 20.9 22.1 10.6 20.9 22.1 10.6 20.9 22.1 10.6 20.9 22.1 10.6 20.9 22.1 10.6 20.9 22.1 10.6 20.9 22.1 10.6 20.9 22.1 10.6 20.9 22.1 10.6 20.9 22.1 10.6 20.9 22.1 10.6 20.9 22.1 10.6 20.9 22.1 10.6 20.0 20.9 22.1 10.6 20.0 20.9 22.1 10.6 20.0 20.9 22.1 10.6 20.0 20.9 22.1 10.6 20.0 20.0 20.0 20.0 20.0 20.0 20.0 2	50		3.		- 1	. 1		• 1	1:	. 1	9 1	. 1
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6 25.6 16.7 36.9 42.3 22.5 11.6 8.2 13.2 12.5 23.8 26.3 30.2 30.1 18.2 41.8 48.3 27.7 30.2 30.2 30.1 18.2 41.8 48.3 27.3 12.9 9.1 14.1 15.1 27.7 30.2 30.2 30.2 48.7 56.8 45.3 16.5 11.7 16.7 25.1 42.7 30.2 30.2 48.7 56.8 45.3 16.5 11.7 16.7 25.1 42.7 41.9 46.9 8 45.3 16.5 11.7 16.8 21.8 90.1 140.2 72.4 41.9 69.8 45.3 16.5 13.6 18.6 37.6 61.4 52.0 61.4 52.	54	2	S	3	7.				12.4	•	•. O	
18.0	56	S.	9		2	2			m .		٠ ا	
## 16.5 11.7 16.7 25.1 42.7 41.9 ## 16.9 45.3 16.5 11.7 16.7 25.1 42.7 41.9 ## 16.9 45.3 16.5 11.0 19.2 13.6 18.6 37.6 61.4 ## 16.1 194.0 162.4 23.7 16.8 18.6 37.6 61.4 52.0 ## 16.2 19.2 19.2 13.6 18.6 37.6 61.4 52.0 ## 16.3 19.2 19.2 19.2 19.2 19.2 19.2 ## 16.3 19.2 19.2 19.2 19.2 19.2 19.2 ## 16.3 19.2 19.2 19.2 19.2 19.2 ## 16.3 19.2 19.2 19.2 19.2 19.2 ## 16.3 19.2 19.2 19.2 19.2 ## 16.3 19.2 19.2 19.2 19.2 ## 16.3 19.2 19.2 19.2 ## 16.3 19.2 19.2 19.2 ## 16.3 19.2 19.2 19.2 ## 16.3 19.2 19.2 19.2 ## 16.3 19.2 19.2 19.2 ## 16.3 19.2 19.2 19.2 ## 16.3 19.2 19.2 ## 16.3 19.2 19.2 ## 16.3 19.2 19.2 ## 16.4 19.2 19.2 ## 16.5 19.5 19.5	58 60	0 9	æ 0		e 9	t 7	۲°		4 N	• •	٠. ٩.	
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ROAD DIMENSIONS FOR WATERSHED MANAGEMENT ROAD DIMENSIONS FOR WATERSHED MANAGEMENT ROAD DIMENSIONS FOR SLOPE STAKING AND END AREAS ROAD DIMENSIONS FOR WATERSHED MANAGEMENT ROAD DIMENSIONS FOR SLOPE STAKING AND END AREAS ROAD DIMENSIONS FOR SLOPE STAKING AND END AREAS SC = SLOPE DIST. TO TOP CUT SC = SLOPE DIST. TO TOP CUT WH = TOT. WIDTH DISTURB. HOR. WS = TOT. WIDTH DISTURB. SLOPE STAKE C = CUT HEIGHT C = CUT HEIGHT C = CUT HEIGHT A = END AREA OF CUT - SO. F		. 6	i n	• 0	, L	. ~	. 6	• 6	0 00	, ,	ة . بسر إ	
NO DIMENSIONS FOR WATERSHED MANAGEMENT SF = SLOPE DIST. TO TOE FILL SC = SLOPE DIST. TO TOP CUT WH = TOT. WIDTH DISTURB. HOP. WS = TOT. WIDTH DISTURB. SLOPE STAKE FROADENT ROADENT SC = SLOPE DIST. TO TOP CUT WH = TOT. WIDTH DISTURB. SLOPE STAKE FROADENT SC = SLOPE DIST. TO TOP CUT WH = TOT. WIDTH DISTURB. SLOPE STAKE FROADENT STAKE FRO		63.	0	61.	94.	62.	3	9	•	0	40.	8
SC = SLOPE DIST. TO TOE FILL SC = SLOPE DIST. TO TOP CUT SC = SLOPE DIST. TO TOP CUT WH = TOT. WIDTH DISTURB. HOR. WS = TOT. WIDTH DISTURB. SLOPE STAKE FROM STAKE FROM STAKE FROM STAKE FROM STAKE TO C = CUT HEIGHT STAKE FROM STAKE TO TOP CUT STAKE FROM STAKE TOP CUT STAKE FROM ST	0 0 0 1 1 0	AD DIMEN	IONS FO	ATERSHE	ANAGE	 	O A	IMENSI	S FOR S	ESTAKING	NO END A	EAI
C = CUT HEIGHT CUT SLOPE A = END AREA OF CUT = 50. F		DE WH		F = SLOP C = SLOP H = TOT• S = TOT•	DIST. TO DIST. TO WIDTH DIS WIDTH DIS H OF FILL	E FILL P CUT B. HOR. B. SLOP	+ u→	1 101 1	SC T	= SLOPE = SLOPE = CUT H = HOR.	DIST. T DIST. T EIGHT DIST. CU	TOE FILL TOP CUT STAKE TO
	11	3		C = CUT	EIGHT	5	1	\	DAYLIGHT STAKE	END A	DISTO FI	SO. F

ROAD GEOMETRY DATA USING A 1.5 TO 1 FILL SLOPE

	110000000000000000000000000000000000000		***********								
RCE	SF	SC	I	SM	J-	٦٥	U	Ŧ	ls.	Ŀ Ŧ	A
_				11.8	1.0		9.	•	9.	. ●.	•
12					1.3		Φ.	•			
14			12.7				6.	•	6.		9
		•		8			•	•			•
B 0				•			٠ . ئ		7.1		
02	0 " /	0.0	14.3	14.0	2.5			7.7	7 • T		
				5	2.8		1.7				7.7
54			15.6	9							
56				16.9							
28		9.3	17.2	-							
30					4.7						
32	0	10.5	19.2	1 0							
34	0		0	•				10.4			
36	_			3							
38	-	N	٠ ص	4				• •			2
			ريا	9	8.6	-			8 • 4		
	1 .	5.1	27.0			10.6	5.9				5.
	S	9	6	2				5			7
46			32,3	S	12.8	3		_	7.1	15,7	20.1
	6	0	S	6	- 6			8			3.
	1.	3.	0	. 4		œ		0		6	7 •
52	24.6	9	5.1		20.4	2.	2	3	1.	2.	2
54	œ	-	2			9	4 •	7.	3	ິດ	α.
26	34.4	7.	2.	1.	C	32.8	18.2	32.3	16.8	0	
58	2°	9	9		38.6	•	3.	6	-	7.	0
99	55.9	0	100.0	116.6	51.9	9	-	-	8	48.2	1.
	80.6	87.5	42.	68.			6.	4.		00	19.
64	2	54.		9	38	150.1	83	29.	76.		216.6
99	æ.	623	000	198	C	-	3	20	9	.62	93°
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	ROAD DIMEN	SIONS FOR	WATERSHED	MANAGEMENT	1	ROAD	DIMENSION	S FOR SLO	PE STAK	AND END A	REAS
1	BRADE WH	170	8 8 11 12 8	DIST. TO DIST. TO WIDTH DIS	E FILL P CUT B. HOR			SC STAKE	SP II	0157, TO 0157, TO E1GHT	
1	ROAD THE TANK		WS = TOT. LF = LENGT LC = LENGT	WIDTH DISH OF FILL H OF CUT	TURB, SLOPE SLOPE SLOPE	STAKE	ROAD FILL SEASON	GRADE DAYLIGHT STAKE	HC = HOR. F = FILL HF = HOR.	DIS HEI DIS	STAKE TO
1	\		-00								

ROAD GEOMETRY DATA USING A 1.5 TO 1 FILL SLOPE

ROAD WIDTH = 11 FEET

CUT SLOPE = VERTICAL

1	SF	SC	I	WS	LF	LC	O I	OI	la.	HF.	i
	6.0	6.0 6.0	11.9	12.0	1.1	9.0	9.	5 5 5	9.2	4.9	
		6.1	•		9.0	φ _ε ς	φ.		6.0	0.	
		7.0			1.0	9 -	0 -				
		9.3				1.2	1.2				
					2.8		1.4				
						1.5	1.5				
			3	•							
	α α • υ	6.8	14.3	14.8	4.4	2°0 2°0	2.0	5 5 5	2.4	20 0 0 0 0 0	
1	8.9	6.9	15.1	15.8	4.9	2.1		5,5	1 .		
				4		Ė	•	•		•	
	0 0	7.2		17.0	200					10.5	
	0										
			7 .		7.3						
1			1.	19.2	α	1 .			4.5		1
	2.		8	0							
	13.2	8.0							5.5	13.8	
	4 °		0	2.	11.1						
	5		-	3°	•						
1				25.7						17.3	
				7	16.2					8	
	21.2	9.5	9.92	30.4			4.5		10.4	21.1	
					\mathcal{C}						
	29.0		3.	38.9						-	
	6.			6	1 4				19.1	4	
			25	9	4	5.9	6.0	ហ្វ	27.4	46.6	
	111.3	12.1	102.	123.	c				61.3		
1	ROAD DIMENS	SIONS FOR	WATERSHED	MANAGEMENT		POAD	DIMENSION	S FOR SLO	PE STAKING	AND END AF	REAS
-1	GRADE WH DAYLIGHT		D1 B1 B1	JIST. TO	FO.		1	7 10	= SL0P = SL0P = CUT	0151. TO	T0E
— <u> </u>	ROAD FILL TO SE		WS = TOT. WILE = LENGTH	OF FILL	STURB. SLOPE L SLOPE SLOPE	FILL STAKE F	ROAD FILL TAKAGE	GRADE	HC = HOR. F = FILL HF = HOR.	DIST HEIG DIST	STAKE STAK
	1		-	CHT		1		STAKE	L N	AREA OF	1

10 1	۵	1.8		•					• •				6.6			12.5		14.7		7	œ.		5.	29.5	S.		TOE FILL TOP CUT STAKE TO CL STAKE TO CL - SQ. FT.
SLOPE = .10	Ų. I				7.6	1			X (V)			•	11.7	2.1	3,	13.9	4.	9	7 .	6			1 4	47	0	D E	DIST. TO DIST. TO EIGHT DIST. CUT HFIGHT DIST. FIL
CUT	L -	9.	6.		1.6			•	2 00		•		4 .1			5.6		. 1			•		16		(2)	STAI	SF = SLO SC = SLO C = CUT HC = HOR A = FIL
	ΗĊ	5.6		•	• •	i •			5.7			•	0 1 0			5.8		0		•	•	0.0		6.1	•	S FOR SLO	SC STAKE SC STAKE GRADE DAVLIGHT STAKE
	U	9.	6	0	1.3	1.4		•	2.0				2.9			3.5		• 1			•	ທ ທ ວ ຸ ຸ ຸ		6.3		I Z I W I X	######################################
1	LC	9.	0.	0 • 7	1.1		1.6		2.0				6.2					• 1				5.1		6.3		POA	i -u-\
	F.	1.1	1.6	•	N 100	2.8			4 4 C 4		ກຸກ		7.4			•	11.3	•	14.4	9	6	22.6 27.5	1 6	0	. 4		TOE FILL TOP CUT TURB. HOR. TURB. SLOPE SLOPE
	S.A	200	8	2	13.5	3.1	14.2	•	15.1 15.5	i •	9	· 0		1 6	C		3.		9	œ	-	50	1 &	64.0	7 .	GEME	DIST. TO DIST. TO AIDTH DIS AIDTH DIS A OF FILL A OF CUT
	3	12.0			• •	13.5			14.5	15.3	•	•	• •	8	00		C	2	3	2		30.3	41.0	53.	_	WATERSH	SF = SLOPE SC = SLOPE WH = TOT 0 WS = TOT 0 LF = LENGT LC = LENGT C = CUT HI
1 FEET	SC			•	2 4				7.0		•					8.3		• 1		6		10.1	11.0		12	SI	
WIDTH = 1		6.0			7.0				• •							3	14.5	5	7.	6			37.2	52	4 .	OAD DIM	GRADE WH GRADE STAKE TO FILL TO STAKE T
ō i	SLOPF								300	32				42										99		0 0 0 0 0 0 0	

ROAD GEOMETRY DATA USING A 1.5 TO 1 FILL SLOPE

5 TO 1	V		•						6.7					11.2	• v c	. 4	5.	6	œ	0	22.2	1 -	-		PEAS TOE FILL TOP CUT STAKE TO C	STAKE TO - SO. FT.
SLOPE = .25	<u> </u>	4°9					•		2.6				13.8	12.5	•		•	7.	6	-	25.0	36,1	1.64	105,3		DIST
S IND		9.	0,0		1.4			• •	2.5			•	• • !	4.6	•					1.		1 6		66.5	E STAKING SF = SLOPE SC = SLOPE C = CUT H HC = HOR.	1 H H
	HC	5.7	•	• 0					0.9				6.3	•	•		•				6.9		7.2	7.5	S 1 3 1	GRADE DAYLIGHT STAKE → + HC →
	U	9.	6.	0	1.3		9.0		2.1				3.0				•		- 9				7.0	7.9	ROADERLESION	SF
0 0 0 0 0 0 0 0	٦٦	νοα	σ,		1.3		•		2.1				• •	3.3	•			•			5.7	1 .		-!	ROAD PILL FILL STAKE F	1
	ا ا	1.1		• •	ر. ار.	1 0			4.5	1 0		0	7.5	4.0	•	1 0 0		14.8	7 •	6	m ∞	36.8		- !	10E 10E URR.	
	S.38		12.7	• •					15.9			• a			- 0	4 .		7.	6	2	50	6.05	67.	135.1	MANAGEMENT DIST. TO DIST. TO WIDTH DIST WIDTH DIST	OF CUT
	3				• •	13.7	14.1		15.3			•	• •	18.8	•		5	4.	• 9		1.6	9.	57.0	112.8	MATERSHED SF = SLOPE SC = SLOPE WH = TOT WS = TOT	C = CUT
	SC	6.1	•		• •		200		7.3			•	8 8						10.1		10.9	1 .	12.9	14.3	SIONS FOR	
I	S							D (7)	• •		6	• ·	• •	20	, ,		9	7 .	6	· N	N O	1 80	24.	120.8	GRADE WHORNERS STAKE	SFWS
∝ 1	SLOPE		14	c a	50	22	24	c a	30	32	34	5 K	400	24									64		<u> </u>	

ROAD GEOMETRY DATA USING A 1.5 TO 1 FILL SLOPE

ROAD WIDTH = 11 FEFT

CUT SLOPF = .50 TO 1

10 10 10 10 10 10 10 10 10 10	12 12 13 13 14 14 16 17 18 19 19		28 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	100 100 100 100 100 100 100 100 100 100		9-6	0 0 0 4 0 a	1.8
2 6.3 6.3 12.6 6.5 6.5 13.0 6.5 6.5 6.5 6.5 6.5 6.5 6.5 6.5 6.5 6.5	12. 13. 15. 16. 17. 18. 19. 20.					~ 6		
6 6 5 6 5 6 5 6 6 6 6 6 6 6 6 6 6 6 6 6	13 13 14 14 15 16 17 18 18 19					2,		
6	13. 14. 15. 18. 19. 20.						•	,
7.2 6.9 13. 6.9 7.2 14. 6.9 7.2 14. 6.9 7.2 14. 6.9 7.2 14. 6.9 7.2 14. 6.9 7.6 15. 7.6 15. 8.0 7.6 15. 8.1 7.8 15. 8.1 17. 8.2 17. 8.4 17. 8.7 18. 9.3 8.7 18. 9.3 20. 11.7 9.0 19. 6.1 17. 8.7 18. 9.6 5. 17. 8.7 18. 9.6 5. 17. 9.6 5. 18. 9.6 5. 19. 10.3 22. 10.3 23. 10.7 24.	14 15 15 16 18 18 19					1.0	•	•
7.5 7.0 14.4 6.0 10.7 2.1 14.4 6.1 17.1 10.7 2.2 18.9 11.0 6.0 19.0 6.0 11.0 6.0 6.0 11.0 6.0 6.0 11.0 6.0 6.0 6.0 6.0 6.0 6.0 6.0 6.0 6.0 6	15 15 16 17 18 19 20		1	1	i	1.6	• •	
7.8 7.2 14.8 8.1 7.6 15.8 8.5 7.8 15.8 15.8 15.8 15.8 17.8 11.0 8.7 18.9 11.1 2.5 9.9 2.2 18.9 11.1 2.6 2.3 2.3 2.3 2.3 2.3 2.3 2.3 2.3 2.3 2.3	15 16 16 18 18 20					1.6	1 0	1 4
8 8 1 7 4 15 8 8 5 7 6 15 8 9 7 8 15 9 8 8 7 16 10 4 8 8 7 18 0 11 7 9 0 19 2 12 5 9 3 20 4 13 4 9 9 22 8 15 6 10 3 22 8 15 6 10 3 23 0 17 1 10 7 24 1 18 9 11 1 26	15 16 17 18 18 20					1.8	• •	
8.5 7.6 15. 8.9 7.8 15. 9.3 8.0 16. 9.8 8.2 17. 8.1 17. 9.0 19. 8.4 17. 8.7 18. 11.7 9.0 19. 8.6 17. 11.7 9.0 19. 8.7 18. 11.7 9.0 19. 8.7 18. 11.7 9.0 19. 8.7 18. 9.0 22. 9.0 10.7 24.	16 16 18 19 20 20							
2 9.3 8.0 15.6 15.6 11.0 26.5 23.0 11.0 2.5 23.0 23.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25	16. 118. 119. 20.					2.3		
2 9.3 8.0 16.0 16.0 8.4 17.0 8.7 18.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19	17. 18. 19. 20.	1			•			7.0
4 9.8 8.2 17. 6 10.4 8.4 17. 8 11.0 8.7 18. 11.7 9.0 19. 2 12.5 9.3 20. 4 13.4 9.9 22. 8 15.6 10.3 22. 0 17.1 10.7 24. 2 18.9 11.1 26.	18. 19. 20. 21.						9.8	
6 10.4 8.4 17. 8 11.0 8.7 18. 11.7 9.0 19. 7 13.4 9.6 21. 6 14.4 9.9 22. 8 15.6 10.3 23. 0 17.1 10.7 24. 2 18.9 11.1 26.	18. 20. 21.			•				•
8 11.0 8.7 18.9 11.1 26.5 23.9 11.1 26.5 24.6 10.7 24.6	20.							6.3
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2 12.5 9.3 20. 4 13.4 9.6 21. 6 14.4 9.9 22. 8 15.6 10.3 23. 0 17.1 10.7 24. 2 18.9 11.1 26. 4 21.0 11.6 28.	21.		•		7.2	4.3		
6 14.4 9.6 22. 8 15.6 10.3 23. 0 17.1 10.7 24. 2 18.9 11.1 26. 4 21.0 11.6 28.		•						
6 14.4 9.9 22. 8 15.6 10.3 23. 0 17.1 10.7 24. 2 18.9 11.1 26. 4 21.0 11.6 28.		7.6						13.2
2 10.7 24. 17.1 10.7 24. 2 18.9 11.1 26. 4 21.0 11.6 28.	24.		4.6		7.6		14.5	•
2 18.9 11.1 26. 4 21.0 11.6 28.	25.	12.2				•		•
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21.0 11.6 28. 6 23.9 12.2 31.	30	•				•	00	00
23.9 12.2 31.		18.0					•	ċ
				0.9	8,5	11.7	23.0	
8 27.7 12.8 35.	*07	ů.				•	•	3
33.1 13.6 40.	4	70.0٤	7.8	• 1		17,1	31.1	28.5
2 42.0 14.5 48.	56			7.6	9.3			~ ⊘ a
6 133.4 17.7 126.	151.	132.5		• •	• •			σ.
AD DIMENSIONS FOR WATERSH	ED MANAGEMENT		AD	NS	FOR SLOP	E STAKING	D END AR	EAS
RADE WH SF = SI. SAYLIGHT SC. AAVE HAVE SC. WH = TO.	OPE DIST. TO OPE DIST. TO T. WIDTH DIST	90 B B B B B B B B B B B B B B B B B B B	+	300	STAKE	SF = SLOPF SC = SLOPE C = CUT H HC = HOR.	DIST. TO DIST. TO EIGHT CUT	TOE FIL TOP CUT STAKE T
00 = 0 St	NGTH OF FILL NGTH OF CUT	LOPE	STAKE	-SF	GRADE DAYLIGHT STAKE		HFIGHT DIST. FILL RFA OF CUT	STA

		WIDIH = II	1 EEE 1							5 100	LOPE = ./5	101
10 6.1 6.2 12.4 12.4 1.1 1.0 6.1 6.1 1.1 7.1 7.1 7.2	St. OP						L C	U				٩
Color Colo		•	•	•	•	1.1	8 0		•		•	•
7.5 7.6 154 155 2.6 11.1 6.7 1.6 8.3 1.1 7.6 1.2 6.4 1.2 7.6 4.2 7.6 4.2 7.6 1.2 6.4 1.2 7.6 4.2 7.6 1.2 7.6 7.6 1.2 7.6 7.6 1.2 7.6 7.6 1.2 7.6 7.6 1.2 7.6 7.6 1.2 7.6 7.6 1.2 7.6 7.6 1.2 7.6 7.6 1.2 7.6 7.6 1.2 7.6 7.6 1.2 7.6 7.6 7.6 1.2 7.6 7.6 7.6 1.2 7.6 7.6 7.6 7.6 7.6 7.6 7.6 7.6 7.6 7.6		• -	•	•	•	1		9			•.	
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ROAD GFOWETRY DATA USING A 1.5 TO 1 FILL SLOPE

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ROAD GEOWETRY DATA USING A 1.5 TO 1 FILL SLOPE

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ROAD GEOMETRY DATA USING A 1.5 TO 1 FILL SLOPE

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ROAD GEOMETRY DATA USING A 1.5 TO 1 FILL SLOPE

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I I	3.0 13	3,3	3.5	3.8 14	• •	14.7 15.1	5.1 IS.	4. V A	6.2	6.7 17.	7.2 18.	7.8 18.	10.	• 02 0 • 6	9.8	0.6 22.	1.6 23.	2.7 25.	•0 26•	5.5 28.8	7.4 31.2	9.8 34.2	0 38	25.6		WATERSHED MANAGEMENT	SF = SLOPE DIST. TO TOE SC = SLOPE DIST. TO TOP WH = TOT. WIDTH DISTURB. WS = TOT. WIDTH DISTURB. LF = LENGTH OF FILL SLOP
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ROAD GEOMETRY DATA USING A 1.5 TO 1 FILL SLOPE

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WIDTH = 12	SF	\$ \$ \$ \$					•			9.0						13.1		15.0		17.7	6	-		33.6	42.3	.65	- 1 -	GRADE WH- GRADE WH- STAKE FILE FILE STAKE STAKE WHO STAKE STAKE WHO STAK
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ROAD GEOMETRY DATA USING A 1.5 TO 1 FILL SLOPE

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CUT S	14	r- 8	•	•	1.0			•	9.0	• 1	•		0.4	•				6.9	•		10.1	-		9	20.3	9		- 1	E STAKIN	SF = SLOPE SC = SLOPE C = CUT H HC = HOR. F = FILL HF = HOR.	
	웃	6.5		•						•			9 0	•	. 1			6		0			11.9	Š				9	S FOR SLOP	SC STAKE SC STAKE GRADE DAYLIGHT STAKE	
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OAD DIM	IONS F	i <	VAGEME		10	ENS	S FOR SL	OPE STAKING	D END A	E
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ROADER S.F. WS		WS = 101. LF = LENGT LC = LENGT	WIDTH DIN OF CUI	ISTURB. SLOPE L SLOPE F SLOPE	FILL F RO	ROAD FILL TORGOLD	GRADE GRADE DAYLIGHT	HC = HOR. F = FILL HF = HOR.	DIST HEIG DIST	STAKE TO . STAKE TO

ROAD GEOMETRY DATA USING A 1.5 TO 1 FILL SLOPE

ROAD WIDTH = 12 FEFT

CUT SLOPE = 1.5 TO 1

IC F HF A	.1 14.2 1.3 .7 7.1 2.1 2	.6 14.7 1.5 1.6 .9 7.4 .8 7.3 2.	.3 1.8 2.0 1.1 7.7 1.0 7.5 3.	.8 16.0 2.2 2.4 1.3 8.0 1.2 7.8 4.	4 16.7 2.6 2.8 1.5 8.3 1.4 8.1 4.	۰۲ (۵۵ (۱۰۵ (۱۰۵ (۱۰۵ (۱۰۵ (۱۰۵ (۱۰۵ (۱۰۵	7.9 18.3 3.4 3.7 2.1 9.1 1.9 8.8 6.	8.8 19.3 3.9 4.2 2.3 9.5 2.2 9.2 7.	9.7 20.3 4.4 4.8 2.7 10.0 2.5 9.7 B	.7 21.5 5.0 5.4 3.0 10.5 2.8 10.2 9.	1.8 22.8 5.7 6.1 3.4 11.1 3.1 10.7 10.	3.1 24.2 6.4 6.9 3.8 11.8 3.5 11.3 12.	4.5 25.9 7.2 7.8 4.3 12.5 4.0 12.0 13.	6.1 27.7 8.1 8.8 4.9 13.3 4.5 12.8 15.	7.9 29.9 9.2 9.9 5.5 14.3 5.1 13.6 17.	.0 32.3 10.4 11.3 6.2 15.4 5.8 14.	2.4 35.2 11.8 12.8 7.1 16.6 6.5 15.8 22.	5.3 38.6 13.4 14.6 8.1 18.1 7.4 17.2 25.	.7 42.6 15.4 16.7 9.3 19.9 8.5 18.8 28	2.9 47.5 17.8 19.3 10.7 62.1 9.9 60.8 33.	8.0 C.0.5 C.0.1	4.5 61.5 24.5 26.6 14.8 28.1 13.6 26.4 46.	3.2 71.8 29.5 32.0 17.7 32.6 16.4 30.5 55.	.0 86.0 36.3 39.4 21.9 38.8 20.1 36.7 68.	2.3 105.1 44.3 50.2 27.9 47.6 25.1 44.5 10.0 139.9 62.3 67.5 37.5 62.2 34.5 57.8 1	71.4 201.7 91.9 99.7 55.3 89.0 51.0 82.5 172.	00.0 356.2 166.0 180.1 99.9 155.8 92.1 144.2 311.	00.00 1437.8 684.9 742.9 412.1 624.1 379.9 575.9 128	ATERSHED MANAGEMENT ROAD DIMENSIONS FOR SLOPE STAKING AND END AREA	SF = SLOPE DIST. TO TOE FILL SC = SLOPE DIST. TO TOP CUT WH = TOT. WIDTH DISTURB. HOP. WE = TOT. WIDTH DISTURB. SI OPF EM. C = CUT HEIGHT
SC			•	•	œ o	• i			10.6	11.2	11.9	12.6	13.5	14.4		16.8	00	20.1		• 1 t	6.12		7	4 6	70.00	1 4	85	748	NSI	000000000000000000000000000000000000000
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8	е Ф		34.7		26.1				• 4	æ	7
0	34.2	11.7	39.4	46.0	31.7	0 1	0 1		7.	2	30.
2	42.8		9	55.1					2		(7)
49	60.1	13.0		73.1	58.4		7.0	6.5	32.4	55,1	
9	131.5	14.3	_	1					N	15	\$
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ROAD GEOMETRY DATA USING A 1.5 TO 1 FILL SLOPE

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3 A MEL 1 A MEL 1 A MER 1 A ME	22.6 26.7 32.5 41.8 60.0 134.7 134.7 134.7 188. HOP. PB. SLOP	31.2 33.8 37.1- 41.4- 26.7- 47.4- 32.5- 57.0- 150.9-	27.7 29.7 33.8 37.1 35.8 41.4 26.7 40.7 40.7 40.7 40.7 40.7 40.7 40.7 41.8 63.7 75.6 60.0 125.9 150.9 150.9 150.9 134.7 F = SLOPE DIST. TO TOE FILL C = SLOPE DIST. TO TOP CUT H = TOT. WIDTH DISTURB. HOP. S = TOT. WIDTH DISTURB. SLOP F = LENGTH OF FILL SLOPE C = CUT HEIGHT

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	3	14.2				15.8	16.2		•	18.0	1 80	6	,	21.3	in	°,	* U	27.1	28.9	31.1	ر س	37.6	51.1	67.3	ATERSHED	SF = SLOPE SC = SLOPE WH = TOT • U WS = TOT • U LF = LENGTI C = LENGTI
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ROAD GEOMETRY DATA USING A 1.5 TO 1 FILL SLOPE

CUT SLOPE = .50 TO 1	WS LF LC C HC F HF A	.5 1.3 .8 .7 7.6 2.	.9 1.6 1.0 .9 6.9 .9 7.8 3.	.3 1.9 1.2 1.1 7.0 1.1 8.1 3.	5.7 2.2 1.4 1.2 7.1 1.2 8.4 4.	.1 2.6 1.6 1.4 7.2 1.4 8.7 5 3 1.7 9.0 5		7-1 3-4 2-0 1-8 7-4 1-9 9-3 6-	7.1 3.9 2.2 2.0 7.5 2.1 9.7 7.	8.3 4.4 2.5 2.2 7.6 2.4 10.1 8.	9 2.6 7.8 3.0 11.0 9.	101 3.1 4.5 9.7 9.9 11.5 10		1.5 6.7 3.8 3.4 8.2 4.2 12.7 13.		4 9.2 4.4 3.9 8.5 5.1 14.2 15.	5.7 10.3 4.7 4.2 8.6 5.7 10.3	7.1 11.5 5.1 4.6 8.8 6.4 16.0 18.	8.8 12.8 5.5 4.9 8.9 7.1 17.2 20	0.6 14.4 5.9 5.3 9.1 8.0 18.5 21.	2.8 16.3 6.3 5.7 9.3 9.0 20.0 24.	5.5 18.5 6.8 6.1 9.5 10.3 21.9 26.	8.6 71.3 7.3 6.5 9.8 11.8 24.2 28.	2.6 24.8 7.9 7.0 10.0 13.8 27.2 31.	7.9 29.6 8.5 7.6 10.3 16.4 31.1 35	5.2 36.3 9.2 8.3 10.6 20.2 36./ 39.	6.7 47.1 10.1 9.0 11.0 26.1 45,7 45.	.1 68.5 11.2 10.0 11.5 38.0 63.5 53.	8.6 156.6 12.9 11.5 12.3 86.9 136.8 67	NT ROAD DIMENSIONS FOR SLOPE STAKING AND END AREAS	. TO TOE FILL . TO TOP CUT . TO TOP CUT	
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10	7.2	7.5	9.41	14.7	1.3		7.	7.1	7.6	7.6	
				15.6	6.1	0 0	-		1.1		0
				16.1			1.3		1.3		
				16.6	5.6		ស្តា ក				
	8.6		16.8	17.1	0	0 1		. 1	1 . /	0 1	. 1
			17.3	17.7							
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	9°8		18.4							0.	0
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36	0	0	8	6	7.0		3.7	9.3		\sim	
38	3°	-	9	4 .							S
40				26.2			•		0	4	9
42	5		5	7.	10.7			0	0		6
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46	17.9	13.4	28.4	-			5.6	10.7		-	
48	6	4 •	0.	3				-			0 47
	21.4	14.7	2	9				0	0	0	-
	6		4	6	6		9	9	11.0	2	6
	9	16,3	7 .					12.3	2	9. M	3
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5.00 m	35.4		46.6	53.9		11.6	۳°6	13.4		33.2	41.1
		19.8	53.7	2 1	0 1	= 1	. 1	0	2	• 1	:
		21.4		76.1	0	4	-	5.	00	0	-
64	9		86.1	\sim	76.4	_	12.7	16.1	45.4	70.	9
	∞	~	172.1	.90	-	8	5	•	9	0 4	9
		SIONS FOR	WATERSHED			ROAD	DIMENSION	IS FOR SLO	STAKI	AND END AF	REAS
	GRADE WH GRADE DAYLIGHT STAKE	0	SF = SLOPE SC = SLOPE WH = TOT. WS = TOT.	I C M	TOE TOP URB.	0 ← <u>u</u> →	PIONO FILL TO MORO	SCUT SC STAKE	S = SL C = SL C = CU	DIST. TO DIST. TO DIST. TO DIST. CU	00 -
1	SF_WS	\	C = LENG	H OF CU	07	1		DAYLIGHT STAKE	11 11	DIST	STAKE TO
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ROAD GEOMETRY DATA USING A 1.5 TO 1 FILL SLOPE

V V	3.2				i i		- 00 - 00		11.0		m I	s v	18.3	0	5	6.46	•	- 1	4	6 4	† -	59.4	0	87.9	122.	N .	
Ŀ.H	7.6			• •	1	້ວ	10.3	. •		11.9			14.9	15.9	7.	18.4	20.0	-	9	27.1	e. D (Ŋ	4	182.2	AND END ARE	151, TO 151, TO 6HT 5T, CUT 16HT 5T, FILL A OF CUT
	7.	1.1	1.3	1.5	1	•	າ ດ		3.2				្ត ទ				δ.	. 1	-	رص ،	0 0		2	48	117.1	E STAKING	W W I
HC	7.3				i i					•		•	11.4			13.0		14.4		16.1	•	19.8	1:	24.2	28.3	S FOR SLOP	SC STAKE SC STAKE GRADE DAYLIGHT
	ဆီဝ	1.1	1.3	1.5		0	0 0		3.1	9		•	6.4			9 i	•	0				13.3		17.7	21.8	DIMENSIONS	SF SPANOR FILL
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	1.3	1.9	2.3	20.7		ر د د	t 4	5.3	5.7	6.4	7.2		10.1	11.3	12.7	14.3		18.5		24.8			00	88.1	- 1		TOE FILL TOP CUT TURB. HOR. TURB. SLOPE SLOPE
SM	14.9	15.9	16.4	17.0		13.0		20.8	21.8	2	• 4	5 4	-	10	32.2	34.6	7 .	40.5	4	φL	n	73.8	90	123,5	252.2	MANAGEMENT	DIST. TO DIST. TO VIDTH DIS VIDTH DIS VIDTH DIS VIDTH DIS VIDTH OF FILL
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SC	7.7		8.4	& & & &			0.0		•	•	-	n n	13.3	14.0		15.6	9		80	0,	- (75.9	. 00	32.8	39.6	SIONS FOR	1/57
S	7.3			∞ ∞ 4 ∞			10.0		11.1		•		15.0		7.		e c	22.9	5.	oc r	• •	47.8	62.0	06	212.7	ROAD DIMEN	RADE WH AVLIGHT TAKE FILLS FILL SF WS
SLOPE PERCENT	10	14	16	208		25	56	28	30	32	34	36 36				94						09		49			

RCENT	S	SC	3	S	 	ا د د		IC	i	Ŧ	۷
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c					3.2	3.5	1.9				
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9	0	-	Į.	Ĉ.				0 °			
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9	14.4	15.6	ဆိ	0	α. α.	6	5,3	14.4			
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2	04.	113.7	55	1.39		08	59.	6		99	02.
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99	47.	-	300	557.	0	90	46.	16	11.	23.	1509.
0 0 1 1	AD DIMEN	TONS FO	ATERSHED	MANAGEM	! !	io	DIMEN	S FOR SLO	STAKIN	ND END A	
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	ROADE FILL EAST		S = T0T	WIDTH DISH OF FILL		STAKE	ROAD FILL TO EACH	GRADE	2 []	ST. CUT	STAKE T

ROAD GEOMETRY DATA USING A 1.5 TO 1 FILL SLOPE

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0.6 8	5 8	0	8	• 4	. 4
	OAD DIMENS	IONS FOR SL	E STAKIN	ND END AR	EAS
FILL CUT		E STAKE	SF = SLOP SC = SLOP C = CUI	DIST, TO DIST, TO EIGHT	OF CU
SLOPE E E	-u-	GRADE DAYLIGHT STAKE	F = FILL F = FILL F = HOR.	DIST. CUI HEIGHT DIST. FILL REA OF CUI	STAKE TO
	2 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	4.2 4.3 4.3 4.2 4.5 4.8 5.9 4.8 4.8 8.0 5.1 5.1 0.6 5.4 5.4 3.8 5.7 5.7 8.1 6.1 6.1 4.2 6.5 6.5 0.6 8.5 8.5 HOR. FILL FOLD DIMENS E STAKE FROND FILL FOLD FI	2.7 4.3 4.3 7.0 4.5 4.5 7.0 5.9 4.8 7.0 0.6 5.4 5.4 7.0 3.8 5.7 7.0 4.2 6.1 7.0 7.0 7.0 8.5 7.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8	2.7 4.3 4.3 7.0 7.0 7.9 4.2 4.5 4.5 7.0 7.9 8.0 5.1 5.1 7.0 10.0 0.6 5.4 5.4 7.0 11.4 3.8 5.7 5.7 7.0 113.2 8.1 6.1 6.1 7.0 13.2 8.2 7 5.4 7.0 113.2 8.1 6.1 6.1 7.0 13.2 8.2 7 7.0 13.2 8.3 8 7.0 7.0 13.2 8.5 8.5 7 7.0 19.0 8.5 8.5 7 7.0 7.0 78.0 8.5 8.5 7.0 7.0 78.0 8.5 8.5 8.5 7.0 78.0 8.5 8.5 8.5 7.0 78.0 8.5 8.5 8.5 7.0 78.0 8.5 8.5 8.5 7.0 78.0 8.6 8.5 8.5 7.0 78.0 8.7 0 7.0 78.0 8.7 0 7.0 78.0 8.8 0 7.0 7.0 78.0 8.9 7.0 7.0 78.0 8.9 7.0 7.0 78.0 8.9 7.0 7.0 78.0 8.9 7.0 7.0 78.0 8.9 8.5 8.5 7.0 7.0 78.0 8.9 8.5 8.5 7.0 7.0 78.0 8.0 8.5 8.5 8.5 7.0 7.0 78.0 8.0 8.5 8.5 8.5 7.0 7.0 78.0 8.0 8.5 8.5 8.5 7.0 7.0 78.0 8.0 8.5 8.5 8.5 7.0 7.0 78.0 8.0 8.5 8.5 8.5 7.0 7.0 78.0 8.0 8.5 8.5 8.5 7.0 7.0 78.0 8.0 8.5 8.5 8.5 7.0 7.0 78.0 8.0 8.5 8.5 8.5 7.0 7.0 78.0 8.0 8.5 8.5 8.5 7.0 7.0 78.0 8.0 8.5 8.5 8.5 7.0 7.0 78.0 8.0 8.5 8.5 8.5 7.0 7.0 78.0 8.0 8.5 8.5 8.5 7.0 7.0 78.0 8.0 8.5 8.5 8.5 7.0 7.0 78.0 8.0 8.5 8.5 8.5 8.5 7.0 7.0 78.0 8.0 8.0 8.0 8.5 8.5 7.0 7.0 78.0 8.0 8.0 8.0 8.5 8.5 8.5 7.0 7.0 78.0 8.0 8.0 8.0 8.5 8.5 7.0 7.0 78.0 8.0 8.0 8.0 8.0 8.0 7.0 7.0 7.0 78.0 8.0 8.0 8.0 8.0 8.0 7.0 7.0 7.0 78.0 8.0 8.0 8.0 8.0 7.0 7.0 7.0 78.0 8.0 8.0 8.0 8.0 7.0 7.0 7.0 78.0 8.0 8.0 8.0 8.0 7.0 7.0 7.0 78.0 8.0 8.0 8.0 8.0 7.0 7.0 7.0 78.0 8.0 8.0 8.0 8.0 7.0 7.0 7.0 78.0 8.0 8.0 8.0 8.0 7.0 7.0 7.0 78.0 8.0 8.0 8.0 8.0 7.0 7.0 7.0 78.0 8.0 8.0 8.0 8.0 7.0 7.0 7.0 78.0 8.0 8.0 8.0 8.0 7.0 7.0 7.0 78.0 8.0 8.0 8.0 7.0 7.0 7.0 7.0 78.0 8.0 8.0 8.0 7.0 7.0 7.0 7.0 7.0 78.0 8.0 8.0 8.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7	2.7

Y I	WID1 = 14	- - - - -									
SLOPE PERCENT	SF	SC	I	S	<u>Н</u>	۲c	U	F.		#	A
	7.6	7.7	15.2	15.3	1.4	m (100	7.1	æ. 0	89	2.9
	6	0	•	•		٠, ١	٠.			0.	•
19	• •	0 °	0 0	16.3	4	1.5	4 (F) • •	7.1	• C	0. 0	
						1.4			1.5		
20		8.2		-	3.2	1.6	1.6	7.2	1.8		•
		8.3		•							7.1
	6			œ							
26	10.0	8.6	18.0	18.6			0	•			8.7
30	00		18.5	6 6	л.1 6.1	4 9 .	4.0		3.1	11.2	10.6
32	11.4		10	10	1 1	1 0	1 4	1 4	1 4	1 - 4	11.5
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36	2			2							13.7
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04			2.	3°			3,7	7.4			
	14.9	0	3	1 10						15.7	7.
	9	10.3	9	9							æ
	17.1	0		27.7	12.9		4.4			17.7	20.3
84	80	0	26.5	6				7.5	•		2
50	20.1	11.2	90	•	16.2			9		0 1	9
52	N	11.5	6	(7)	19.3				0	2	5
54	24.5	11.9	2.		21.0			7.6	-	4	œ
	7.	5	4 .	6	• 4				3	~	0
58	31.8	13.4	38°54 63°8	44.6 51.1	7.88.7	0°9	4 ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° °	7.6	19.4	30.9	33.5
62	ir	14.0	10						1 4	1 4	
49	66.5	4		-	9	0 0	0	7.8	0.1	0	47.3
99	9	0	2	8	S				0	127.7	
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	ROAD DIMEN	SI	TERSH	NAGEM	8 8 8 8 8 8 8		DIMENSION	S FOR SLOP	E STAKING	AND END AR	EAS
<u> </u>	WH LIGHT CE		SF = SLOPE SC = SLOPE WH = TOT• WS = TOT•	IST. TIST. TIST. DIDING	0 TOE FILL 0 TOP CUT STURB. HOR.		THE STATE OF THE S	SC STAKE	SLO SLO CUT HOR	DIS DIS EIGH DIST	
	ROAD TRA	*	= LENGT = LENGT = CUT H	OF FIL	DPE DPE	STAKE	SF	GRADE DAYLIGHT STAKE ←HC→	= FIL = HOR = END	HE DI	STAKE TO
	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		8 8 8 8 8 8 8 8 8			9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9		9 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	

ROAD GEOMETRY DATA USING A 1.5 TO 1 FILL SLOPE

ROAD WIDTH = 14 FEET

CUT SLOPE = .25 TO 1

ENT	SF	0 1	II.	S/A	LL I	L C	0	UI	La. 0	- Ia. I -	
	7.7	7.8	15.3	15.4	1.4	3°0 1°0	ಹ ರ್	7.2	w 0°	0.0	
				16.1		1.1	1.1		1.1	- B	7
	4.8	8.1		16.5		1,3	1,3		1.3		7
	0.0	& & % & &	16.7	16.9	& W & W	1.5	1.5	• •	1 . 0 . 0 .	0°9 7°6	υæ
1		1 4		17.9		1	1	1 4	1		
	7.6	0 00 1 00 1 00 1 00 1 00 1 00 1 00 1 00	17.9		4°1		2.0	7.5	2.3		- 00
	_			6	4.6				16		6
	_	0.6	18.9	0	5.1						6
	11.0			0	5.7		2.7		3.2	. •	10
1	11.6	4.6	20.0	21.0	6.4			7.7	0	. •	11
		•	0	-	7.1						13
	2		•	2	7.8					3	14
	13.5	10.1	22.1		8.7			7.9		14,2	15
	4		3	24.7						ů.	16
1	5	10.7	3) . o.	
	9		5	1						9	
	7		26.2		13.2		4.7	80	7.3		21
			-	•	•					19,3	23
	20°1	12.0	29.5	32.7	16.7	5.5		• [. 1	•	
	2	•	-						10.5	2	
	25,3	12.8	33.5		-				12.0	S.	
	8	13,3	9	41.9	25.1				3	-	32
			0	.9		7.2	7.0	8.7		31.8	36
	39.2	14.6	46.1	53.8	36.4				0	7.	39.
	6			64.8	9	•					
	9	16.5		86.	67.	6	6°8	9.5	•	63	51
		18.2	•	° N	152.7			6	0 1		
1	DAD DIMEN	S I 0	ATERSHE	ANAGEME	9 9 9 9 9 9 9 8 8	ROAD	DIMENSION	S FOR	E STAKIN	2	EA
	PE K		11 11	DIST. TO	F O			E STAKE	= SL0P	DIST. TO DIST. TO	1
	STAKE LF FILL TO STAND		WH = 101. WS = 101. LF = LENGT	WIDTH DIS WIDTH DIS H OF FILL	TURB. HOR. TURB. SLOPE SLOPE	STAKE F PO	ROAD FILL FOLLOW	GRADE	# # FILL	EIGHI DIST. CUT HEIGHT	STAK
1	CA/					1		STAKE	:	1000)

						9				m 4					0									מ מ			0	1	FILL CUT E TO CL, KE TO CL
0 TO 1	A	2.				n vô		&		10.	iN	(9	18.	6	-	23.	25	27.	0			41.	in	J	78.		10E 10P STAK STAK
OPE = .50	Ŧ		9,4	•	٠. 🗨	9. 9	į . e.			11.4	1						7.	18,5	6	-	3	9	6	33°5 39°6	10	0.00	147,3	ND END A	DIST, TO DIST, TO EIGHT DIST, CUT HEIGHT DIST, FILL REA OF CUT
CUT SI	L.	80	6		•	0 80				9,0				•				7.7			11.1	ŝ	41	17.7	1 0		93.5	STAKING	SF = SLOPE SC = SLOPE C = CUT HE HC = HOR. E F = FILL H A = END AP
	ų			•		2.9									9.1			9.6	6				•	11.1		• (13.2	S FOR SLOP	SC STAKE SC STAKE GRADE GRADE DAYLIGHT
	ပ	8	1.0	1 ° 1		1.7				2.6					4.2			5.3					•	N 6 8 8	1	•	12.4	DIMENSION	ROADFINIT SE
	٦٦		1.1	 		1.9				3.2														N 0	10		13.9	10	FILL STAKE F
	٦	1.4		•		• •				• •	1 .		8.1			11.1		13.8		•	0	0	• 9	31.9	ic				TOE FILL TOP CUT TURB. HOR. TURB. SLOPE SLOPE SLOPE
	SA		•	-	•	17.9	18.5	19.1	19.7		18	22.9	3	25.1	9	27.7	6	31.0	3°	5	00		S.	51.6 59.5	1 -		N	NAGEME	E DIST. TO WIDTH DIST WIDTH DIST WIDTH DIST TH OF FILL TH OF CUT
	3	15.5		•	° r	17.5	1 8	œ	6	9.	1 .		22.5			25.5		28.1			3	9	0	44°6 51°0	1	9 (ATERSHE!	SF = SLOPE SC = SLOPE WH = TOT. WS = TOT. LF = LENG1 LC = LENG1 C = CUT H
4 FEET	SC		8.1			• •				9.6	10.1			11.1	•		5		13.1		•			16.3	1 0		22.5	SI	
WIDTH = 1	SF			•		9.1			10.3	10.8			3	14.0	+	15.9	7.	18.3	6	21.7	4 0	9	01	35.2	1 6	, in		OAD DIME	GRADE WH GRADE WH STAKE FILL FILL ROAD THE SE
αi	SLOPE PERCENT			5		20	22	54	56	30	32	34	36	38	40			46			52	54	56	58 60	62		99	0 8 0 0 0 1	

ROAD GEOMETRY DATA USING A 1.5 TO 1 FILL SLOPE

SLOPE	S		3	SM	L 1	C	υ	HC	Ls.	7.5	A
					1.4			•	8		
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ROAD GEOMETRY DATA USING A 1.5 TO 1 FILL SLOPE

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19.5 11.2 27.6 30.7 15.2 4.8 21.2 21.2 11.5 29.2 32.6 17.1 5.1 5.1 2.2 32.6 17.1 5.1 5.1 25.1 25.7 12.2 33.3 37.9 22.0 5.8 28.9 12.6 36.2 41.5 22.0 5.8 36.2 41.5 22.0 5.8 33.3 37.9 22.0 5.8 33.3 37.9 22.0 5.8 6.1 33.3 13.0 40.0 46.3 30.1 6.5 6.1 2.6 39.5 13.0 40.0 46.3 30.1 6.5 7.0 20.1 2.6 13.5 45.5 53.0 36.6 7.0 7.5 6.1 2.0 71.5 53.0 36.6 47.0 7.5 7.0 20.1 20.1 20.1 20.1 20.1 20.1 20.1 20	.6 7.	 00	
23.2 11.5 29.2 32.6 17.1 5.1 2.1 23.2 23.2 11.8 31.1 35.0 19.3 5.4 25.7 12.2 33.3 37.9 22.0 5.8 28.9 12.6 36.2 41.5 22.0 5.8 33.3 37.9 22.0 5.8 6.1 33.3 13.0 40.0 46.3 30.1 6.5 33.0 36.6 7.0 40.0 46.3 30.1 6.5 7.0 39.5 13.5 45.5 53.0 36.6 77.0 7.5 69.3 15.0 71.0 84.4 67.4 8.1 7.5 7.0 71.0 84.4 67.4 8.1 7.5 7.0 71.0 84.4 67.4 8.1 7.5 7.5 7.0 70.0 FILL	.8 7.	.4 20.	4
23.2 11.8 31.1 35.0 19.3 5.4 25.7 12.2 33.3 37.9 22.0 5.8 28.9 12.6 36.2 41.5 25.5 6.1 33.3 13.0 40.0 46.3 30.1 6.5 39.5 13.5 45.5 53.0 36.6 7.0 69.3 15.0 71.0 84.4 67.4 8.1 ROAD DIMENSIONS FOR WATERSHED MANAGEMENT ROA	.1 7.	.5 21.	9
25.7 12.2 33.3 37.9 22.0 5.8 28.9 12.6 36.2 41.5 25.5 6.1 33.3 13.0 40.0 46.3 30.1 6.5 31.0 39.5 13.5 45.5 53.0 36.6 7.0 7.0 69.3 15.0 71.0 84.4 67.4 8.1 8.1 51.7 16.5 140.4 168.2 150.7 9.1 ROAD DIMENSIONS FOR WATERSHED MANAGEMENT ROAD TICLE	.4 7.	0.7 23,	8
28.9 12.6 36.2 41.5 25.5 6.1 33.3 13.0 40.0 46.3 30.1 6.5	.8 7.	2.2 25.	0
39.5 13.0 40.0 46.3 30.1 6.5 39.5 13.5 45.5 53.0 36.6 7.0 7.0 49.4 14.2 54.1 63.6 47.0 7.5 69.3 15.0 71.0 84.4 67.4 8.1 51.7 16.5 140.4 168.2 150.7 9.1 ROAD DIMENSIONS FOR WATERSHED MANAGEMENT ROAD ST. SF = SLOPE DIST. TO TOE FILL	.1 7.	4.1 28.	3.
39.5 13.5 45.5 53.0 36.6 7.0 49.4 14.2 54.1 63.6 47.0 7.5 69.3 15.0 71.0 84.4 67.4 8.1 5 151.7 16.5 140.4 168.2 150.7 9.1 ROAD DIMENSIONS FOR WATERSHED MANAGEMENT ROAD			
49.4 14.2 54.1 63.6 47.0 7.5 69.3 15.0 71.0 84.4 67.4 8.1 51.7 16.5 140.4 168.2 150.7 9.1 ROAD DIMENSIONS FOR WATERSHED MANAGEMENT SF = SLOPE DIST. TO TOE FILL	٠/	0.3	40.5
4 69.3 15.0 71.0 84.4 67.4 8.1 6 151.7 16.5 140.4 168.2 150.7 9.1 ROAD DIMENSIONS FOR WATERSHED MANAGEMENT ROA 	.5 7.	6.1 46.	5.
ROAD DIMENSIONS FOR WATERSHED MANAGEMENT	8.1 7.5	63	51,3
DIMENSIONS FOR WATERSHED MANAGEMENT SF = SLOPE DIST. TO TOE FILL	•1 7 •	3.6 132.	2.
SF = SLOPE DIST. TO TOE FILL	AD DIMENSIONS FOR SLOPE	TAKING AND	AS
WIDTH DISTURB. HOR. WIDTH DISTURB. SLOPE FILL SLOPF TH OF FILL SLOPE TH OF CUT SLOPE	ROND FILL TO SE STAKE SC CUT SF SC STAKE SC C C C C C C C C C C C C C C C C C C	= SLOPE DIST, TO = SLOPE DIST, TO = CUT HEIGHT = HOR, DIST, CUT = FILL HEIGHT = HOR, DIST, FILL = END AREA OF CUT	100 - 51

ROAD GEOMETRY DATA USING A 1.5 TO 1 FILL SLOPE

F - - - - - - - - -											
	SF	SC	I	S	1.5	LC	ပ	HC	L.	HF	۵
0 1		•		16.4			8		80		
12				16.7		1.0	1.0		1.0		
71	8°.7			17.1	2.0	1.2	1.2	7.6	1.2		
9			17.3	17.5		1.4	L • I		1.4	•.	
			•	17.9		ហ (•			1.6	•	
20	9.6	80	18.0	18.3	3.4	1 • 7	1 • /	7.7	1.9	10.3	7.3
22			8	œ							
4	10.3		18.8	19.4		2.1			5.4	11.1	
9		9.2	19.3		6.4	2.3		7.7		11,5	10.0
80	11.2		6	20.5				•			11.1
0.	11.7		0	-			2.7	•	3.4		12.1
32	1 4	1 4	10	1:	6.7			1 4		13.1	13.2
			_	~	•	- 1					
36		0	2	m			•	•	•		•
		0		4		•	•	•	•	•	•
	•		3	Ŋ	10.1	3.9	0	7.9		15.9	
42	16.0	10.8	1 4	9	11.2		1 .			16.8	
77			25.8	28.2			4.5	7.9		1	
. 9	8	-	7.	6						6	3.
00		11.7	8	1.							5.
0	Ϊ.	2.	0	3°						•	~
	3.	1 4	1 -	1 9	10	1 4	1 4		10	1 8	16
	9		4		8				2	9	8
9		\mathcal{C}		2.	9			8.1			35.1
	4	3°	-	7	30.8				7.	۰. ص	ď
90	0 1		9	9		7.4	• 1	• 1	20.8	8	
	0	5.	S	5	æ				26.7	7	7
		9		7.			•		8	5.	
99		7.	45.	174。	S	7.6			9		9
ă i	OAD DIMENS		TERSHED		 	ROAD	DIMENSION	S FOR SLOP	E STAKIN	END AR	V
STAY STAY	DE WH	150	0 PE 0 PE 1 T O PE NGT	SET	TOE FILL TOP CUT URB. HOR. URB. SLOPE	← L→	11111111111111111111111111111111111111	25 V	SLO SLO CUT HOR	DIST TO DIST TO DIST. TO DIST. CUT	TOE FIL TOP CUT STAKE T
			C = CUT H	IGHT	5	<u>}</u> ,	\ \	DAYLIGHT STAKE	11 11	- W	- 50. F

ROAD WIDTH = 15 FEET

CUT SLOPE = .25 TO 1

RCENT	SF	SC	3	S	٦٤	LC	C	HC	La.	HF	۵
0		•			1.5	6.	8		80°		
α,			16.8		œ (0 0	1.0		1.0		
÷ u		9	1/01	1.03	V * C	7 .					
D a	•		0,71			1.			•		
0 0	7.6	0.0	18.3	18.6	n € • • •	1.8	 	7.9	1.9	10.90	0.7
	7	0	1 60	19.2		1 .	1 .	1 .	1 4	1 4	1 4
4		6.3		6		2.2		8.0		11.1	6.9
5			6	20.3						-	
m				21.0	5.5						
0	11.8		0	10	6.1	2.9	0	0	3.4		
0				2	δ. Ω.		3.1				13.6
.4		10.3	CJ.	23.4		3.4		8.3	4.2	ص	
9			0	4 °							
ar.		0	3	2						°.	
0	15.4	-	4	9	10.3	•				9	
2	16.4	11.4		1 2	11.4	4.6	4.4	1 .		7	10
.+	~		9	6							8
9	18.8	\sim	8			5.2		8.8	7.9	19,3	4 .
ď	20.3		9	2°						0	9
_	2	2.	1.	5.	7					2	
2		3.	3 1	7.	10					1 4	-
*			5	0	6	6.7				9	4
2	30.6		39.5	• 4	9				• 4	6	7.
œ (35,3	14.9	3			7.7	7.5	4°6	17.7	34.0	41.3
0	42.0		4°67		6			0	-	6	ů.
2	2.	16.5	6	6	0					6	-
4	74.6	17.7	-	2	Ĉ				0	7	6
9	164.7	19.6	53	4	3			0	7°06	3,	73.4
8 8 8		STONS FOR	1 01	GEM				FOR SLO	PE STAKIN	D END AR	
		15/	= SLOPE	IST.	E C			SCOT	= SLOP = SLOP	015T. TO 01ST. TO	
	STAKE LIF FILL SEA SF WS		6.1	TOTH DI	STURB, HOR, STURB, SLOPE L SLOPE SLOPE	FILL	ROAD FILL SEASON	GRADE GRADE	C = CUT H HC = HOR. F = FILL HF = HOR.	EIGHT DIST. CUT HEIGHT DIST. FILL	()
			= CUI H	FIGHT		_		SIMPE	,	DEA OF	00

ROAD GEOMETRY DATA USING A 1.5 TO 1 FILL SLOPE

ERCENT	SF	SC	I A	SM	F-	L C	ပ	HC	 	<u> </u>	d l
			16.7	16.7		6.	80	7.9	8		
12						1.2	1.0		1.0		
14		8 8	17.4	2		1.4	1.2		1.2		6.4
. 91	•		•	æ							
20	8°6	4.6	18.8		3.5	2.1	1.8	•	1.9	•	7.6
			19.3	6							
54	10.6	9.8	6	0							9*6
92											
28	11.6		21.1	21.9	- 6				•		
30		•		2.		3.4	3.0	0.6	3,5		13.1
32	12.7	10.9		3	•					13,3	
34	3		3	4							'n
36	4		4 0	2						. 4	~
38	15.0	11.9			9.6	4.7		9.6	5,3	15,5	8
0+	2		9	8							0
	7			1 6						7.	2:
	8			•				•		. e	4
	19.7	13.5	30.1	33.2	14.8				8.2	6	9
	-	14.0	31.9	2				10,5		l.	6
50	3.			7	19.8	7.3	6.5	• 1	. 1		31.9
	10	•	9	0	-	•			-	TU #	5
24	8	15.9	6	4 .	24.6			11,3	•	8	æ
	2	•	2	6	7.80				ທ	·.	ċ
5.8 5.0	37.7	18.5	47.8	55.2	34.1	9.8	യഹ	11.9	18.9	35.9	47.3
			:	• # • # 1		• i	: ;				1
	51.5	ô,	٠ ک	77.	4	- (0	2	0	~ (0
66 66	181.4	24.1	172.0	102.8 206.0	~ α	12.9	11.5	13,3	100.2		70.7
	OAD DIMEN	SIONS	ERSHED	AGE) i	100	ENSION	S FOR SLO	1 4	END A	EAS
<u> </u>	# # T	1 37	= SLOPE = SLOPE = TOT.	DIST. TO DIST. TO IDTH DIS	E FILL P CUT B. HOR.			SC CUT SC STAKE		DIST. DIST.	TOE FI
1	ROADE HELES		S = TOT. F = LENGT C = LENGT	OF FILL OF CUT	• SLO PE PE	STAKE	ROAD FILL TO THE STATE OF THE S	GRADE DAYLIGHT STAKE	H H H	DIST. CUT HEIGHT DIST. FILL	STAKE T STAKE

SLOPE	SF	SC	I	SM	L. 1	LC	ပ	HC	Le.	4	٩
	88.3	8.7	16.9		•	1.	6-	8.1	8 0	8.7	3.4
	•	•		•		 	4 ° L			•	
14		•	ν « - α	ກ ຕຸ ເປັນ ເປັນ		C &C	 				
	•	9 (ο α				1.7		•	•	. 4
							1.9				• 1
		10.1	0 -	0					•		
			0	-				•			
			ŗ,	0				•	•		•
22 30	11.9	11.0	22°0	22.9 23.8	η φ α 4	3.7	0 m m m	10.0	3°6 9°6	12.9	12.4
		1 4	1 0	1 7		1 4	1 4	1 .		1 .	
	•	•	7		•		1	1	•	. 4	
36		12.6	50°0 50°0	· ·					•	14.9	00
			9	000						5	0 •
			œ	0				11,3		. • [2
	17.8	4		31.9			•	1.	•	7	24.5
	6		1.					2°		6	• 9
94		15.4	32.8	36.1				6		0	6
			•					Š	•	5.	8
	J 1	9	- /	41.7	• 1	• t	• 1		11.0	4 I	9 1
52	~	~		5	8			3.	2	9	6
54	30.7	80	3	6	• 9				•	6	4
56	0	20.0	•	9	0	9		\$ 1	° ,	ຈ. ກໍເ	5 L
-	40.4	22.8	53.8 61.9		37.0 45.8	13.3	11.7	16.3	25.4	45°6	
	63.1	4.	1 4		10	6.	1 .	7.	1 6	1 1	9
94	7.06	7 .	99.3	17		∞		18.5	6.84	0	87.8
	90	31.5	198	7	TC:	21.7		5.0	113.	ထ	7
E 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	OAD DIMEN	IONS FOR	ATER	MANAGEMEI	2 2 3 5 5 5 6 6 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8		DIMENSION	S FOR SLO	PE STAKIN	END	FAS
1	HW TH	0	SF = SLOPE SC = SLOPE WH = TOT. WS = TOT.	DIST. DIST. WIDTH	TOE FILL TOP CUT URR. HOR. URB. SLOPE SLOPE	FILL	ROAD FILLT	SCUT SCUT SCUT SCUT SCUT SCUT SCUT SCUT	F = SLOP C = SLOP C = CUT C = HOR.	DIST. T DIST. T DIST. T DIST. CU	TOP C STAKE
+	SW		C = LENG	H OF CU	L 0 P	1	\	DAYLIGHT STAKE	HOH:	ا ا	SIAKE

ROAD GEOMETRY DATA USING A 1.5 TO 1 FILL SLOPE

10 1	A	3.6	•	0 4	•				9	30	-	e v	30.5	40	ď	2	0 0	0	86	90	135.9	-69			TOE FILE TOP CUT STAKE TO CL STAKE TO C STAKE TO C
OPE = 1.5	Ĭ.	8.8 9.1	•				●.	12.7	•	•			18.3	0 -	ه. او ام اه	9		. e.	8	ທ. ເ		103.1	0 6	ND AR	DIST, TO T DIST, TO T EIGHT DIST, CUT S HEIGHT DIST, FILL REA OF CUT
CUT SL	La.	.8	1.9	• •	2.1	•	•		3.9		•	•	7.2	8.5			• (7.	0	្ធ ហ	32.1 43.2	63.		E STAKING	SF = SLOPE SC = SLOPE C = CUT HE HC = HOR. H F = FILL A = END AF
	HC		60		0	-	•		3.	4.	S	91	19.2	20.8	. d	-	0	5	0	80 (7.27	11.	0,00	IS FOR SLOP	SC STAKE SC STAKE SCRADE DAYLIGHT STAKE
	U	.9 1.1	•		• •		•						7.8	8.9	• (5	00	2.	٠.	34°8 46°8	69	124.9 515.1	D DIMENSION	ROAD FILL TO SE
	٦٦		•	• •	•		•		7.7	•	•	•	14.1	16.0		• •		3	0	6		24	225.1 928.6	OA	FILL
	F .	1.5	•		•		•		7.1			•	13.0	1 4 4	. 0	· N		0	•	S I	77.8	14.	207.5 856.1		TOE FILL TOP CUT URB. HOR. URB. SLOPE SLOPE SLOPE
	SA	1 6	19.2	• 0	•	1 %	4 H	26.9	c	0	2	1 6		44.0	. (89.	07.	7 0	52.	445.2	MANAGEMENT	E DIST. TO WIDTH DIST WIDTH DIST WIDTH DIST TH OF FILL TH OF CUT HEIGHT
	I	17.6	0.0	, 0	0 0	2 -	m :	20.00	-	8	•	o N :	37.5		• •	ິຕ	0	80		93.	115.4	14.	0 1	i Ш	SF = SLOP SC = SLOP WH = TOT• WS = TOT• LF = LENG LC = LENG C = CUT
S FEET	၁Տ	9.6	•	•	11.4		12.5	• •		5	9	œ 0	21.0	22.9	0 1		•	0	9	55.9		1 (1)	231.7	SI	
WIDTH = 15	SF	& & N &	•	, 0			•	12.9			S.	9 1	19.4	21.1	٠ ري ر	00	2	9	3.	51.5	83.9	20.	213.6	OAD DIME	GRADE WH DAYLIGHT STAKE TO FILL ROAD OF THE STAND
	SLOPE PERCENT							82	30				04	42					54		~ ~		499	0 0 0 0 0 0	

ROAD GEOMETRY DATA USING A 1.5 TO 1 FILL SLOPE

SF	SC	I	S	- F	C	U	H	L.	L I	٨
		17.3	7.	1.6				6.	. •.	
		•	7.	1.9	1.0	1.0	•	-		
		17.9		n n	1.2	2.1	•	η• I		•
•	•	•	0 0				•	•	•.	•
	9.5	19.0	0	3.6	1.80	000		0 0 0	11.0	
		19.4	16				1 .		1	9.1
0		6	0	4.6	2.2					
11,3		0				2.4	8.0		12,3	
-		0							. •	
12,3	6.6	-	2	4.4				3.5		
1 2	10.1	1 -	1 6	į (1 - 4	1 4
13.5		i	(1)	7.9			8.0	4.4		16.1
4	0	8	4.							7
5		4.	5.	_						00
	0.				0.4		•	•	•	0
9	11.1	1 10	1 00	11.8					7	2
18.0	11.4		29.3				8.0	7.2	18.9	23.8
6	11.6	8	0						0	2
0		6	5					6	-	7.
2	12.2	-	. 4	•	5.5	5.5	• [9	0
9	•	3.	7.					11.4		S
27.4		S	4004				•		10	S
			44.3	27.2		6.5	8.0	15.1		38.3
ທີ	13.9	2	6	32.1			•		•	
42.1	14.4	8	56.6	39.1	7.4	7.4	• [•	9
	15.1				8.0	8.0		27.8		-
73.	9	75.	90	-	•	9	•	`• •	9	00 (
	17.6	149.7	6 1	160.7	• 1	,-	8.0	. H9.	3 1	0
4	SN	WATERSHED	MANAGEMENT		ROAD	DIMENSIONS	S FOR SLOP	PE STAKING	AND END AR	KEAS
GRADE WH DAYLIGHT STAKE IF FILL TO FIL		SF = SLOPE SC = SLOPE WH = TOT. WS = TOT. LF = LENGT LC = LENGT	DIST. TO DIST. TO WIDTH DIS WIDTH DIS H OF FILL	TOE FILL TOP CUT TURB, HOR. TURB, SLOPE SLOPE SLOPE	+u->	111	SC STAKE	SF = SLOPE SC = SLOPE C = CUT H HC = HOR. F = FILL	DIST. TO DIST. TO EIGHT DIST. CUT HEIGHT DIST. FIL	

SLOPE	SF	၁၄	I	S	ب ا	٦	U	H	le.	<u>L</u>	۵
			17.4		1.6	6.	6.		_		3.8
		•	-	•		1 • I			(°		
	•	•	œ (1.3	7.1			•. 5	•
	•	•	χ (•		† ·	† ·		•	•	
		•	x			9.] • [●.	•
20	70.0		ا 6	19.6	3.6	ρ•Τ	D • I	• 1	• 1	- 1	. 1
22	•		6	0							
54		7.6	20.1	0							
56			0	-							
24		10.0	-							2	2.
30	12.4	10.2	-	22.6	4.9	5.9	5.9	8.3	3.6	13.4	13.6
32	13.0	10.4	2	9						14.0	5
34			~	7		-	-	•	-	. 7	9
36		• •	10	S)			• •			B. 6	-
38			4	9	•		- Te			. 1	6
c		11.3	2	27.3		4.2	4.2	4.8	0.9		
42	17.1	1 .	1	1 8	į (1 0	1 4	1 4	1 4	7	13
	00		-	C		•		- 1	4	6	7
949	6	12.1	00	_		9		. co		20.3	
	-		c	3					- 0		8
	3		2				5.7			3	-
	1 6	1	1 4	ia	1 -	t	1	į i	1 -	i L	1 6
	00	13.6	36.6	•		• •			13,3	27.9	9
56			0			6.9	6.9	8.7	S		
	9		. 4		~					5	3,
	43.1	15.3	50.1	00 i	0				2	1.	9
	54.1	16.0	59.6			0			00	0	4 .
64	.92			93.1	73.9	9.5	9.2	8.9		69,5	
	~		5	10					2	S	S.
	IME	SIONS FOR	ATERSHE			ROAN	DIMENSION	S FOR SLO	PE STAKING	AND END AR	EAS
<u> </u>	RADE WH		= SLOPE = SLOPE = TOT	DIST. TO DIST. TO IDTH DIS	OF CUT	-		STAKE	SF = SLOPE SC = SLOPE C = CUT H	DIS DIS EIGH	TOP CUT
	SF WS		F = LENGT C = LENGT C = CUT H	OF FIL	KK. SLU LOPE LOPE	FILL STAKE	ROADFILLTSE	GRADE DAYLIGHT STAKE	D 11 20 E	DIST. DIST. RFA OF	STAKE STAKE
-											7

ROAD GEOMETRY DATA USING A 1.5 TO 1 FILL SLOPE

ROAD WIDTH = 16 FEFT

CUT SLOPE = .25 TO 1

SLOPE	SF	SC	N	SM	LF	LC	U	HC	le.	HF	A
10	•				1.6				•	9.	
	•	•	•	•	1.9	1.1	1.1		•		
		•	•		۳° ۱	۳, I	۳. ا	•	•		
	•	•	•	•			۲°۱		•	9	
20	10.3	0.0	19.5	19.4	3.6	1.9	1.9	0 00 4 10	2.0	11.0	4 4
22	10.7	1	10			1 4	1	1 4	1 .	1	1
	11,1	6 6	0		4.7					11.9	10.5
	11.6		-	-	_				•		
28	12.1	10.3	•	22.4				8.7		12,9	12.9
30	12.6	10.6		9					3.6	•	. 4
32		10.8	2 :	4	7.3		•				
34			9	4	_						7.
36	14.6	11.3	4		6.8					. •	
38		11.6	5	7					•		0
04	16.4	11.9	9		11.0	4 . 5	4.4		•	17.1	•
42	~	12.2	27.3	6	12.2				•	8	3
44	œ	•	œ	-						6	.0
46	20.1				•		ស រ វ រ	6.0	7. 00 (27.8
1 L	• •			10	0.0	•	•	•	,	, ,	
(' (• ! ? !	• 1	9 1	- 1	. 1	2.0		. 1	. !	0 1	• [
52	9	14.2	5	·	-		•		2	9	35.7
	00	14.7	8	3	7.40				3°	® .	6
	32.6		41.8	47.9		7.7	7.5	6.6	15.9	—	2
	•	15.9	9 0	m,	34.0	•	•		œ (9 0	7.
		16./	2:	-	-		• [0 1		2 1	2
62	•	7	2	4.	8		6	0	6		80
49	79	18.8		0 0	77		10.1		6.24	r 1	67.6
		•		0 1	•	11.0	: 1	9	• 1	9 1	01
	OAD DIMEN	STONS FOR	ATERSHED	MANAGEMENT		ROAD	DIMENSION	IS FOR SLOP	E STA	AND END AR	RAS
	GRADE DAYLIGHT STAKE LF FILL TO ROAD TO		SF = SLOPE SC = SLOPE WH = TOT WS = TOT LF = LENGT	DIST. TO DIST. TO DIST. TO WIDTH DIS WIDTH DIS WIDTH DIS	TOE FILL TOP CUT TURB. HOR. TURB. SLOPE SLOPE	+u+)	ROMO FILL TO SE	SC STAKE	SF = SLOPE SC = SLOPE C = CUT H HC = HOR. F = FILL	015T; T 015T; T 015T; T E1GHT 015T; CU	TOE FILTOP CUT
7	28		C = CUT H	EIGHT	5	<u>}</u>	\ \ \ \	STAKE STAKE	1 11	REA OF	ווי
			0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0					*			

0 TO 1	٩				7.6					• •	9	8	6,	21.5 23.5	1 4	0 1	• -		9	16	3	α		0					TOE FILL TOP CUT STAKE TO CL.
SLOPE = .5(Ŧ	9.3	4. 0	. •		• 1	11,5			13.6		. •	0.	16.5 17.5	1 0	•. o	• -	22.8	. 4	7.	6	3	38.3	2	9	78.2	80	AND END AF	E DIST, TO E DIST, TO HEIGHT DIST, CUT HEIGHT DIST, FILL AREA OF CUT
CUT	L	6.1	• •	•	1.8	• 1	•			3.7			•	5°,7	1	•	•	000		1 %	4	7.		4	32.2	• 9	96	PE STAKIN	SF = SLOPI SC = SLOPI C = CUT I HC = HOR. F = FILL HF = HOR.
	HC HC	80 cc 4 cc					•	•	•	9.6			0	10.2	0	•	•	11.2		11.7		N	12.7		9			ONS FOR SLO	E STAKE SC STAKE SC STAKE GRADE GRADE GRADE HC-
	ပ	-			1.7	. 1				200			•	4 4 V &	1		•	0°0			8.0		6	10.2		12.3		D DIMENSI	ROAD FILL SEF
	L C	1.0	1.0		1.9	. 1	•			3.0				• •	1	•		7.2		1 .				11.4			15.8		STAKE
	LF	1.6	. m	2.8	3.0	3.1	7.4	•		6.7		€. 8.		10.2	10.7		י ע י ע	17.7	0	22.8	9		36.4	44.7	00	84.3			TOE FILL TOP CUT TURB, HOR. TURB, SLOP SLOPE SLOPE
	S	17.9		6	19.9	•	-	- (ů ~	• •	5	9	- (30.00	1 -	٦ ٣	ט ר	37.7	0		7.	8	58.9	œ ˈ	82	6	19.	MANAGEM	OPE DIST. TO OPE DIST. TO OPE DIST. TO OPE DIST. TO OPE DIST. TO OPE DIST. WIDTH DIST. NGTH OF FILL OPE CUT
	3					70.1	• 0	, ,	• ~	• •	1 4	4	s S	27.9	10	• -	• (34.0	9	8	1.	2	51.0	œ 1	6	2.	183.4	WATERSHE	SF = SLOP SC = SLOP WH = TOT. WS = TOT. LF = LENG LC = LENG
6 FEET	SC	0.0			6	• 1	•						o c	13.0	10	• •	9 4	15.0	5.	16.2			8	19.8	1.	22.8	5	NSI	
D WIDTH = 1	SF			•		•	•		17.0	• •			ŝ	17.0	1 0	0	• _	22.7	. 4	27.4	C	. 4		48.2	-	86.	194.1	OAD DIM	GRADE WH GRADE STAKE LF FILL STAKE ROAD SF WS
ROA	SLOPE PERCENT									30								6 4		52	54	26	58	09					

ROAD GEOMETRY DATA USING A 1.5 TO 1 FILL SLOPE

۵	3.9	•					10.1	11.4	12.7	14.2			6	- (25.4	• !	6.72	0	9	~	0	S	°	9 0	71.9	1 6	6	131.1		OF FILL OP CUT TAKE TO CL
¥	9,3			*. O	10.7		11.6	12.0	12,6	13.1		14.4	ទ	S v		•	6	20,3	•	3	5	9	31.4	ر. ال	40°8 48°6	1 -	. 9	189.9	ND END ARE	DIST. TO T 16HT 15HT CUT S EIGHT 1ST. FILL
L. 1	6.	1.1		1.6		0 [2.4			ው ሌ 4 ወ	1				U • 4	• [7.3				11.8		15.6	œ ,	27.1	i u	52.1		E STAKI	SF = SLOPE SC = SLOPE C = CUT HE HC = HOR. D F = FILL H
H	8.7								10.2	0		10.9			100	• 1	12.4	12.8				•	ů.	ů,	16.5	l a	6	,	S FOR SLOP	SC STAKE SC STAKE SC STAKE GRADE GRADE GRADE GRADE GRADE GRADE
U	6.	1.1		1.6		• {				ر د د د د	• 1			•	•	• [6.3					9.5		11.4			18.5	NOI	ROMO FILL SEE
rc	1.1		•			2.6				0°4	9				2.0	• 1	7.3	7.9		9°3		11.0	11.9		14.2		- 0	23.1		FILL
<u>ب</u> ۳	1.6	0.0					4.3	6.4	5.5		• i	7.7	8.6		0 0	• 1	13.2	4 °	ŝ	18.7	21.2				າ ຊາ ເພ	1 0	9 (000		O TOE FILL O TOP CUT STURB, HOR. STURB, SLOPE L SLOPE
SA	18.1			19.8	50.4	21.1	21.8	22.6	23.5	24.4		56.5	27.7	29.1	30.0	u i	34.0	36.1		_	40.44	48.2	2		77.0	10	7 0	253.8		DIST. 1 DIST. 1 WIDTH DI WIDTH DI H OF FILL
N	18.0	00 (6	19.5	20.1	20.7	21.3	22.0	2	23°57	• 1	2	9	~	0 0	• 1	31.4	33,1			39.7		9	51.2	• • • 9	10	90	~	ATERSHE	SF = SLOPE SC = SLOPE WH = TOT. WS = TOT. LF = LENGT
SC	•	7. 6				10.5	10.7	11.1	11.4	11.7					1 t • 0	• 1			16.5		18.1	19.0	20.1	21.3	24.4	1 4	0 0		is	1303
SF	8.9						11.1	11.5	12.1	12.6			•	•	10.0	• 1	18.9		2	4.	26.4		2	7.	43.6 52.7	ir	; ; ;	250.2	AD DIME	GRADE WH DAYLIGHT STAKE NO POLICE ROAD OF THE STANDARY
SLOPE PERCENT				16			22	54	26	28		32	34	36	D C			77	94	48	50	52	24	56	58		2 4	99	1 1 1	

SLOPE			 				U	HCH	L	Ŧ	4
	- 1	- 1	1	Ĺ	I .	1				1	İ
12	5 m	7.0	18°3	e c			1.2	6.6	1.1	n 6	4 4
			6	6							
16			0	20.2	2.8				1.6		
		10.6	.0				1.9		1.8		
20	10.8	11.0	21.3	1 .	8° 8°	3.0					
22	11.3	11.3	N	2				10.4	2.4	11.6	10.5
54	11.8	11.7	2		5.0		2.7	10.7			11.
56			3°	4 .				11.1			
28			J 1		6.3		4°E	11.4		13.2	
30	13.7	13.1	s i	9 1	. 1			11.8	. 1		. 1
32	4	13.7	9	о Ф							
34	2		28.0	29.5				12.6	6.4	15.4	
			6	- (6.6			س		91	o i
	•	15.6	0		•				•		ŝ
	œ 1		2	0 1	12.4	8.6		4	• 1	e	- 1
42	6		4	7 .	13.9					6	0
44			.9	6	5					1.	. 4
94	23.4	19.2		45.6	7 .	11,3	8.0	16.0	9°6	25,6	37.8
48	2°		•	5	20.0			9	11.1	4.	2
50			4.	6	°.			7.	5	9	9
52	-	23.1	8	1 4	1 .	5	0	8	9	6	2
54	5	. 4	\mathcal{C}		0	9	$\overline{}$	9	9	3,	6
56					9	8				38.0	7.
58	8	29.1	9	77.3	8	0		22.6	4	. 4	7.
09	8	-	~		. 4	23.2	9	4	0	3	
62	6	5	95.0	11.	72.4	6	00	6	0	8	07.
64		40.4		0			21.8	29.8	60.	98	
	261.7	e 60	59	10.	59.	-	9	4	. 4	4	85.
0 0 0	AD DIMEN	SI	ATERSH	NAG	9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	ROAD	DIMENSION	S FOR SLO	PE STAKIN	AND END AF	REAS
<u> </u>	RADE WH	1000		01ST. TO	OE FIL	8		SC STAKE	= SLOP = SLOP	DIST. T	TOE FILI
	ROAD FILL STATE		WS = TOT W WS = TOT W WS LF = LENGTH	DTH DIS OF FILL OF CUT	TURB. SLOPE SLOPE SLOPE	FILL	ROAD FILL BASSES	GRADE	• 🔟 •	DIST. CUT HEIGHT DIST. FIL	STAKE T L STAKE
	\		11	FIGHT		_		1	LEND	IN OF AR	00

ROAD GEOMETRY DATA USING A 1.5 TO 1 FILL SLOPE

A		•	•	• 6	c o			13.0	14.8		18.V	•	24.0	27.	30.	3	6	. 4	51.4	6	6	-	8	21.	154.6	07.	06.	554.4	87.	AREAS	TO TOE FILL TO TOP CUT CUT STAKE TO
±	4.60				1000	•	11.8	12,3			5 o t I			17.0			21,1	2	25.1	7.	-	5	•	8	59.4	77.1	10.	192.2	67.	G AND END	11ST. 6HT ST. C
	6.	7 0 1			1.0	• [Z**		5,3						11.4			18.1	-				68.	122.8	90	AKIN	SC = SLOF C = SLOF HC = HOR HF = FILL
H		•		0	11.1	•	12.1	12.7	3		2.41	5		7.	6	0	2	. 4	26.5	6	3°	7.	٠ س	-	63.7		18.	207.8	32.	OR SL	SC STAKE GRADE DAYLIGHT
		•	•				2.7				٥.4		5.8						12.4		16.6	6	3.	9		6.64	73.	ന	•64	MENSI	ROAD FILL TATA CON
C		•						5.6			2.8	2.6		11.7	13,3		7.	6	22.3	5	0	5.	2		7.	0.06	i m	240.1		ROA	STAKE
-J	1.6	0 0 0 II	0		4 0	• 1	4.5		5.9		۲۰۶				12.2			-	20.2		7.16	32.7	0	α		83.0		21.	-		TOE FILL TOP CUT TURB. HOR. TURB. SLOPE SLOPE
MS	18.9	•	•	- (, V C	0 1		25.7	7 .	Ø	30.4	2.	34.5	7.	6	3			56.8		71.6	82.0	5	4 0	45.	186.6	68	47	17.	A GE	E DIST. TO WIDTH DIS WIDTH DIS TH OF FILL
I	18.8	•	•	•	- 0	• 7	6	2	26.2		29.1	0	32.7	4.	7	•	9	7.	51.6	57.1	64.0	2 :	4	00		60	78.	4000	09	ATERSHE	SF = SLOP SC = SLOP WH = TOT WS = TOT LF = LENG LC = LENG
SC	8.6	10.0	•	•	12.0	T • 2 I	12.7	13.4		4	15.8	9	17.9	6	0					33.0		42.7	6	. 6		97.1		247.1	997.5	i =	
SF		•	•		10.7	• 1	11.7	S		e,	14.6		9		6	•	2 .	4	27.3	0	4	39.3	S	5		89.5	29.		-	OAD DIM	GRADE WH DAYLIGHT STAKE LF FILL FOR SF
SLOPE					200		22	54	56	28	30	32	34	36	38	0 4			94						58			49		0 0 0 0	1

							3			0 M				رن د										V O			6	1 1 1	10 CL. 70 CL. 70 CL.
RTICAL	∢						10.	11.	2	14.	1 9		6	21.	n i	4	9	0	(ment)		9	$\boldsymbol{\sigma}$	3	47. 52.	1 ~	5	79.	i W	TOP CUT STAKE TO STAKE TO
LOPE = VE	生		•	•.	•	11.7	12,1	12.6	13,1	13,6	1		0-	17.0	• 1		0	•. —	8	24.6	9	6		43.0	1 0	8	150.6	D END A	DIST. TO DIST. TO DIST. CUT HEIGHT DIST. FILL
CUT S	L	6.	1 • 1	1.4	•	2.1		2.7		9°6				5.7	.	6.9			6			3	9	23.0	16	N	4 •	E STAKING	SF = SLOPE SC = SLOPE C = CUT H HC = HOR. F = FILL HF = HOR.
	HC					• •				യ മ സ സ				ຜູດ	•				•					ສ ຜູ້ ພູບ	1 .		8.5	S FOR SLOP	C STAKE GRADE BAYLIGHT STAKE
	U	6.	1 • 1	T • T	1 0	1.9				2.8 3.0				0.4	0 1									7.9	1 0		10.3	IMENSION	ROAD FILL SE
	٦٦	6		m		1.9				2°8				4 °0 °0 °							•		•	4.7	1 .		10.3	ROAD	FILL STAKE F
# # # # # # # # # # # # # # # # # # #	٦							6.4		6.1 6.8	1 .			10.2		12.5	3		7	6	•	2°	28.9	34.1	53.2	9	0	0 0 0 1 1 1 1 1 1 1	TOE FILL TOP CUT URB. HOR. URB. SLOPE SLOPE
	S 33		18.8	.	•		1 -	21.7	8	3.6	1 4	5.	• 9	27.3	• 0	6	-	2°	4	7 .	6	2		N 0	1 8	95.6	190.	NAGEME	DIST. TO DIST. TO WIDTH DIST WIDTH DIST H OF FILL H OF CUT
8	3	18.4		•	•	0.0	10		-	22.1 22.6	100	8	. 4	25.5	0 1		~ &	9	-	3	5.	7.	•	45.4 51.5	1 -	-	6	TERSH	SF = SLOPE SC = SLOPE WH = TOT. WS = TOT. LF = LENGT LC = LENGT C = CUT H
	SC	•	•	•	•	9.6	1 .		9	10.4			-	1103	-	-	2	12.4	5	3				14.7	16.1	1		SI	
푸	SF				•	10.8	11.2	11.6	12.1	12.6	13.7			15.9				20.5	5		26.3	6	32.8	37.7	56.0	8		OAD DIME	GRADE WH DAYLIGHT STAKE LF FILL ROAD TO SE
	SLOPE	01								30				හ . ග				46						28 60			99	0 6 0 0 0 0	

ROAD GEOMETRY DATA USING A 1.5 TO 1 FILL SLOPE

۷	4.2				• 1	10.5	•		• •	7.	80	0	73.7		٠,			5	9 1		· 0	49.4 54.5	0	69°7	EAS	TOE FILL TOP. CUT STAKE TO CL STAKE TO C
¥	9.9			11.3	• 1	12.1	12.6		14.2		. •	16.3		i	•. • <	70°C	•. • - ←	4	- 2	6	۳,	37.5 43.9	3.	73	• I Z	DIST. TO DIST. TO DIST. TO DIST. CUT HEIGHT DIST. FILL
L_	1.1	1.4		2°0	•				9 ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° °				5°,7		0.0		7.6		12.4	14.1	16.4		10		STAKI	SF = SLOPE SC = SLOPE C = CUT H HC = HOR. F = FILL HF = HOR.
HC	8 8 6			8.7	• j	8.7		•	0 00				D	i i		0 0						E 6		0 0	S FOR	CUT SC STAKE SC STAKE CRADE DAYLIGHT
	1.1	1.3	1.5	1.7					3.1													æ. . æ.		6 -	DIMEN	ROAD FILL TAKES
r C	1.1	1.3		1.7	•				3.1				4 4 7 10	1		ر 1 م			6.5			8 * 4			•	FILL
<u>1</u>	1.7		5.9	m 0	•	7.4		•	. vc		8.4	6.6	10.3		7.00	14.1	17.5	19.7				42.5	4 .	78.5	0	TOE FILL TOP CUT TURB. HOR. TURB. SLOPE SLOPE
SA	18.6 19.0	6	6	20°3	•	21.3	•	2		1 4	5.	• 9	0.68	1	• o •		٠ د د	9	10	4		3 C	1 4	9 6	6EME	DIST. TO DIST. TO DIST. TO MIDTH DIS MIDTH DIS MIDTH DIS H OF FILL
3	18.5 18.8	6	6	0	• !	20°8	.	- 0	23.0	3	4 •	2	0 1	1	° 0	7 0	,	4	1 9	8	5.	9 m	3.	83	RSHE	SF = SLOPE SC = SLOPE WH = TOT • WS = TOT • LF = LENGT LC = LENGT
SC	6 9 8			8°60	•	10.1	•	10.4	• •	11.0	11.2		12.0	1			13.2		14.0	14.5	15.0	16.2	17.0	1861	SIONS	
SF	99.3				•	11.2	11.7	12.1	13.2	3	•	S.	16.1		0 0	1 4° C.C.	. ~	4.	9	29.7	٠ ص	_	57.5	900	OAD DIME	GRADE DAYLIGHT STAKE STAKE NOAD FILE ROAD SF
SLOPE PERCENT				28					30				38 04			† ¢						58 60		79		

			8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	8 8 8 8 8 8	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	8	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0			
SLOPE PERCENT	SF	၁၄	3	S	L.F.	٦٦	ပ	HC	la.	¥	Ø
100	9.9	4.6	18.6	18.7	1.7	1.0		7.88 7.88	6.	6.6	4 n
	• (. 0	. 6		• (• (• 1	7 .		•
16				C			1.6		• •		• •
		•	0	0					1.9		
	0	• (0		•	•		•	•	. •	
				-	•						10.7
	11.8		•	2°							11.9
		•	2	3.							
30	12.8	11.0	22.9	23.8	0 v v	3.3	3.0	9.5	ທຸດ ທຸດ	13,7	14.6 16.0
32	1 .	1 .	- 4	1 .		1 4	1 0	1	1	1 4	
34			. 2	•	•		. (1	•		6
3.6			5			4.2		9.5	•	9	0
38	9		9		c					7.	2
40	•			30.0	11.7	•		•	6.5		
	80	•	6		12.9					6	
	6	13,3	0		14.4		- 4			0	
94	21.3			35.0	16.1	5.9	5.7	6.6	8,9	-	31.4
	3°	4 •	33.5		18.0					8	
	5	14.6	2					•	-	o.	
52		•	7.	2	22.9		6.9	10.2	12.7		0
54	30.7		40.7	9	9			10.4	14.6	.0	. 4
26	4.	9	4 •			8.2			9	3	48.2
58	0		6	9	9					8	3.
9	47.6	17.7	56.0	65.4	44.2	•	•	10.8	24.5	9	
62		00	9	00						. · S	9
64	∞		8	4		-	0	11.2	5	76.8	76.3
99	7	2.	4	96	5	12.6	0	-	2	2	. 4
0 0 1 1 1 1 1	D DIMEN	SIONS FOR	ATERSHED	NAGEM		ROAD	DIMENSIONS	FOR SLO	PE STAKING	AND END AR	EA
	GRADE DAYLIGHT STAKE	1 33	= SLOPE = SLOPE = TOT =	DIST. TO DIST. TO WIDTH DIS	TOE FILL TOP CUT TURB. HOR. TURB. SLOPE	← L-	ROADFILL	SC STAKE	SF = SLOPE SC = SLOPE C = CUT H HC = HOR,	E DIST, TO E DIST, TO HEIGHT DIST, CUT	TOE FILL TOP CUT STAKE TO CL
	SFWS	-\	C = LENGT C = CUT H	H OF CUT	0	1-1	-SF /	GRADE DAYLIGHT STAKE	H H	DIST	STAKE TO - SQ. FT.
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8		0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1					

ROAD GEOMETRY DATA USING A 1.5 TO 1 FILL SLOPE

				8 0 0 0 0 0	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1			1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1			
OP	SF	SC	13	S	LF	٦٦	U	HC	la.	Ŧ	<
	4.6	9°6	18.9	6	1.7	1.1	1.0		6.		
2			6	6	2.1	1.3	1.2		1.2		
4	10.0	10.0		20.0	2.5	1.5				10.6	
9	10.3			20.5		1.8	1.6		1.6		
6 0	10.7		0	21.1					•		
0	11.1	10.6	21.3	21.7	3.9	2.3	2.1	9.5	•	11.8	
2		10.9	-								
4	12.0	11.1	0								12.4
2		11.4	3.		5.7			6°6			
90	13.1	11.7	23.9	24.8				0.			5
0	13.7	12.0	4.	5	7.1	•	3.4		3.9	14.4	
	1	1 4		1 9	7.9	1 4		10.4	1 4	1 .	1 8
4	15.2		9	1	•				•		0
. 9	•		~	6				0		•	2
m			00	0				0			4
0		13.9	6			5.8	5.1	11.1	6.7	18.6	26.5
2	0	1 4	-	1 6	13.5			11,3		1.6	
.4	0	14.8	32.5	35.5			0.9	11.5	8°3		
5	2.		4 •	7.				-		2	
ď	4		9	c	80				0	. 4	
Û	9		∞	2	1.	•	7.4	2.		• 9	•
	6	- 2	41.1	46.4	1 4			2	ا ا	00	45.0
4	2	18.0		0	-					1.	
9			80		6		9.2	3	18.0	35,5	
œ	2		•		34.7	-		3		•	60.7
0	51.2	21.0	61.9	2		12.1	0		9	œ i	68.1
2	4	2	74.2	7.		3.		4.	4.	6	7
4	92.	4 0		16.				5	6		
9	90	27.3	194.9	33	204.8		15.1		113.6	178.9	115.0
8 8 9 8	AD DIMEN	015					DIMENSIONS	S FOR SLOPE	STA	ND A	REAS
	WH ADE WH	1/3/2	= SL0 = SL0 = T0T	DIST.	TOE FILL TOP CUT TURB. HOR.	-		SC STAKE	SF = SLOPE SC = SLOPE C = CUT H	DIST. DIST.	OF FI
1	ROADER SF WS	1	5 = 101. 7 = LENG 7 = LENG 6 = CUT	OF FIL	ISTURB. SLOPE LL SLOPE F SLOPE	STAKE	ROAD FILE SE	GRADE DAYLIGHT STAKE	FILL HOR.	DISI. CUI HEIGHT DIST. FILL	STAKE TO
1)	4				_	2021	7	2

ROAD WIDTH = 17 FEET

CUT SLOPE = .75 TO 1

	SF		3	S/A	L F	L C	0	HC I		I	A
		9.8	19.1		1.7	1.52	1.0	9.5	1.2		
		0	0	0		•			•		
		00	0,	· .						•	
	11.3	• •	2 .	22.4	4.0		2.2		2.2	11.8	10.1
		11.4	1 8	3.1	1 0			0			
			3	. 4				0			12.8
		2	. 4	6 4				0	•		4.
28 30	13.4	12.5			7.3		3.4	11.3	3.6	13.9	16.0
32	14.9		1 .	1 00	1 .	1 .					10
34	15.7	3		6				-			
36	9	4.		0				2°			3
	17.6	14.8 15.4	30.3 31.8					12,5		0. 0	
42	20.1	16.0	3.	6.			1 .	3.	1 .	10	1:
77	21.7		S	8	15.7			3.		, o.	. 4
9	23.4				7	9.1		14.0			00
80	25.5	œ	6	6	19.9	6		4.		். மி	-
50	e		2	2			• 1	4.	SI	7.	9
52	-	0 -	45.5		5	11.7		_	14.3	0	— V
1 9	•	• (•		• r L			0 \	•	9 1	•
0 00	7 (. v		 V C	n -	0		0 1	9 (ا. ه س	າ ກ
09	. o l	25.9	70.2	81.8		16.6	13.3	18.5	• •	e. e	• •
	7	i 00 c	48	100	67.9	18.5	14.8	_	7	1 W	94.
99	33.	o .	25.	69	2	4	0	٠ (٣)	28	0. 0	1 49
1 1 1 0	OAD DIME	SIONS F		NAGEMEN	1		DIMENSION	S FOR SLOP	E STAK	ND END A	EAS
1	GRADE WH DAVLIGHT STAKE ROAD FRILL ASS		SF = SLOPE SC = SLOPE WH = TOT. WS = TOT. LF = LENGT LC = LENGT C = CUT H	DIST. TO DIST. TO WIDTH DIS WIDTH DIS H OF FILL H OF CUT	TOE FILL TOP CUT TURB. HOR. TURB. SLOPE SLOPE SLOPE	+4+	ROAD FILL TO SE	SC STAKE SC STAKE GRADE GRADE DAVLIGHT STAKE	SF = SLOPE SC = SLOPE C = CUT H HC = HOR. F = FILL HF = HOR.	DIST. TO DIST. TO EIGHT DIST. CU HEIGHT DIST. FI	TOE FILL TOP CUT STAKE TO STAKE T

ROAD GEOMETRY DATA USING A 1.5 TO 1 FILL SLOPE

10	SF	SC	3	SM	le.	٦٦	U	HC	la.	1	Ø
			16				1.0		6.		
			0	0			1.2		1.2		
	10.2	10.6	0	0	₽•5			10.0	1.4	10.6	9.9
			1.	•		•		•			
				8					•		6
	11.5	11.6	2	23.1	4 • 1			10.8	•	11.9	10.4
		2				3.7					11.9
			• 4	5.				11.4		12.9	13.4
	13.1		25.2	9	6.0			11.8		13.5	
		3.	9	7.		•					16.8
		14.0	7	28.5			4.0	12.5	4.2	•	
	1 4	- 7	1 0	6		1 .	1 4	12.9			20.8
	16.2	S	0	-				•		. •	3.
		5	-	3	- 4						S
	•	9	2	٠ ک	4	•				80	00
	19.7		4	1	13.2	•	6.5	15.0		19.5	-
2	1 7	1 4	1 9	16	14.8	1 4	1 4	1 4	1 .	10	1 4
1 7	2	6	00	,	• (•				2	a
9	24.8	7000	-			12.1	8.5		0		42.7
8	7.	•	4	8					-	• 9	7
0	0	3°	4-14	3°	4			18.8	•	8	3
	16	- 7	1 -	1 &	27.8	1 0	1		1 5	1 :	10
7	7	9	9	47			-	-	8		9
9		00	N		00	0	13.9		21,3	0	•
80	1.	0	1,	2	9	-		4	5	7	7
0	2			9	• [• (17.5	9		. • (- i
2	-	7	000	18.	7 .	iοο	6	00	2	2	21
1 99	•	-	136.0	161.5		32.7	23.1		63		150.3
9	00		75.	29°	76.	•	8	-	3	38	.60
ROA	D DIMENS	i —	ATERSHED	MANAGEMENT	R 0 1 0 0 0 0	ROAD	DIMENSION	IS FOR SLOP	E STAKIN	AND END AR	EAS
SRAC	7 7 1	1 1/35	= SLOPE = SLOPE = TOT.	DIST. TO DIST. TO IDTH DIST	TOE FILL TOP CUT URB. HOR.			C STAKE	17 11 11	DIST, TO DIST, TO EIGHT	TOE F.I
THE OWNER OF THE OWNER O	FILL SE ST		S = TOT. F = LENGT C = LENGT	DTH DISTOF FILL OF CUT	URB. SLO SLOPE SLOPE	STAKE F RO	ROAD FILL STA	GRADE DAYLIGHT STAKE	HC = HOR. F = FILL HF = HOR.	OIS HEI DIS	STAKE TO STAKE TO

SLOPE ERCENT 10 12 14 16 11 18	S										
		SC	3	SA	F-	LC	U	HC	L	HF	Ø
	9.6	10.5	0	20.1	1.7			10.1	1.0	6*6	
			0	50.9	2.5		1,3	10.4	1.2		
	•	•	-	21.7	5.6			10.9	•	10,7	
	6.01	11.8	2	22.1		0	•	•	•		
	1.9	12.3				0 0		12.3	0 m N N	12.0	11.2
22 1	12.5	13.5	5 1	6.						12.5	1 -
24		14.2	9	7.				13.5			
26 1			27.9	39							
30	5.5	15.8 16.8		30.4	7.1	7.7 8.7	44	14.9	4.4	14.4 15.2	18.9
32 1	16.5	17.9	2.	34.3	0.6	9.8	1 .	16.7	1 .	16.0	24.
	7	6	4	9				7	•	- 4	7
36	00		37.0	39.3	11.5	12.5	6.9	18.9	4.9	18.1	
	0	0	6	2				0		6	. 4
	5	3°	2.	5	14.7	15.9		1.		. • [9.
2	3.	25.9	5	6	16.7	18.1	10.0	3	6.3		4.4
7	9	ě	0			0		5			0
2 94	6		54.8	0	1.	23.7	13.1		0	26.7	58
8	2°	5.	0	7		7.					7
0	9		8	• 9	4.65	31.9		5.	9		00
2			7	87.1			20.9	39.9	19.3	37,4	2
54 4			6	101.7	-	5.	2°	9	3.		-
9	8	3		121.8		55.8					136.
60	o.	78.	30.	151.2	S.	71.1	36.5	2.	9	63.1	174.5
60 60	95.1	103.2	170.0	198.3	88.2	95.7	53.1	88.1	8 1		234.
2		148.7	42.	2		41.	78.	26.	72	16,	9
Š	2.0	262.	5	2040	35.		141.5	0		204.5	62
9	77.1	1059.8	0	2036.9	970.3	5	83.	884.2	38.	15.	81.
ROAD	DIMENS	ONS FOR	ATERSHE	NAGEME		Ö	DIMENSI	OR SL	TAKIN	END A	⋖
I AAA	WH GHT		SF = SLOPE SC = SLOPE WH = TOT.	DIST. T DIST. T WIDTH DI	2E F	8 8 8		SC STAKE	= SLOP = SLOP = CUT	E DIST. TO E DIST. TO HEIGHT	TOE FIL TOP CUT
ROADE	W.S.		TOT. LENG	WIDTH H OF F	£0.0	FILL STAKE	ROAD FILLT TATABLES	GRADE	۰ ـ ـ ـ ۰ ۱۳۰۰	DIST. CUT HEIGHT DIST. FIL	STAKE T
			81	IE I GHT			HF	-HC	END	AREA OF CU	- 50

ROAD GEOMETRY DATA USING A 1.5 TO 1 FILL SLOPE

8 9 8 9 8 9 9 8 9 9 9 9 9 9 9 9 9 9 9 9	19.5 20.2 20.5 20.5 21.4 22.8 22.8 24.0 24.6	19.6 20.4 20.8 21.3 22.9 22.9 24.3 25.0	1.8 2.0 3.0 3.5 5.5		ပ	HC	L		⋖
10.1 10.4 10.7 10.0 11.0 11.0 12.3 12.8 10.7 12.8 13.9 11.0 13.9 11.0 14.5 11.0 15.2 11.6 16.0 17.9 12.5					1.0	0.6			
10.4 10.7 10.7 11.0 11.4 12.3 10.7 12.8 13.3 11.0 13.9 11.6 16.0 17.9 12.5 19.0				1.2				10.8	
11.0 11.0 11.6 12.3 10.7 12.8 10.7 13.3 11.0 13.9 11.0 14.5 11.6 16.0 17.9 12.5				\$ V	-	0 0	•	7. II.	ο α
11.4 10.4 11.8 10.5 12.8 10.8 13.9 11.0 14.5 11.4 16.0 11.6 17.9 12.2			b	• •		0 0	0 0	•. •	
11.8 12.3 10.7 12.8 10.8 13.3 11.0 13.9 11.2 14.5 11.4 15.2 11.6 16.0 17.9 12.2	1			2.0	2.0		2.2	12.4	10.
12.3 12.8 13.3 11.0 13.9 11.2 14.5 11.4 15.2 11.6 16.0 17.9 12.0 17.9									11.
12.8 13.3 11.0 13.9 11.2 14.5 11.4 15.2 11.6 16.0 11.8 16.9 12.0 17.9 12.5									12.
13.3 11.0 13.9 11.2 15.2 11.6 16.0 11.8 16.9 12.0 17.9 12.5				2.7	2.7	0.6			14.
13.9 11.2 14.5 11.4 15.2 11.6 16.0 11.8 16.9 12.0 17.9 12.2							•	14.4	15.
14.5 15.2 11.6 16.0 11.8 16.9 12.0 17.9 12.5						• (17.
15.2 11.6 16.0 11.8 16.9 12.0 17.9 12.2				3.5	•			5	ac.
16.0 11.8 16.9 12.0 17.9 12.2 19.0 12.5								. 9	0
16.9 12.0 17.9 12.2 19.0 12.5			9.8		4 • 0	0.6	5.4	17.1	22.
17.9 12.2 19.0 12.5		28.9	0					®	
19.0 12.5	6.72	30.1						œ i	in i
			13.2				•	0	27.
20.2 12.8								•	30.
21.7 13.1	-	34.8	9	5.5	5,5	0.6	6	N .	
23.4 13.4	33.2		ď				10.1	4	S
5.4 13.8	35.0	39.2	20.5	•		. 1	-!		37.
27.8 14.2	37.3		23.2				2	00	-
0.9 14.6		45.5	26.4				14.7		44.
34.7 15.1	43.5	6	30.6	7.4	7.4	0.6	17.0	34.5	48.
9.9 15.6	48.1	2	9				20.0	٠. 6	S
47.4 16.3	54.6		44.0		• 1	• 1	4 1	2	58.
59.3 17.0	6.		56.4				1	5	4
.2 18.0	•3	01.	80.8	7.6	7.6	0.6	44.8		73.
192.1 19.7 1	4.89		0		• 1		0	6	6 i
AD DIMENSIONS FOR W	ATERSHED MA	ANAGEMENT			DIMENSIONS	FOR S	E STAKIN	A O	EA
SF SRUIGHT SC SC	SLOPE D SLOPE D	IST. TO T	OE FILL OP CUT	1 1 0 1		5	= SLOP = SLOP	DIST, TO	TOE FIL
	= 101 • WI = 101 • WI = LENGTH = LENGTH	DIH DISTUR OF FILL SU OF CUT SI	IKB. HOK. ILOPE LOPE	FILL F RO	ROAD FILL TEACOR	GRADE	HC = HOR. F = FILL HF = HOR.	DIST. CUT ! HEIGHT DIST. FILL	STAKE

ROAD GEOMETRY DATA USING A 1.5 TO 1 FILL SLOPE

SLOPE ERCENT	le S	၁ၭ	3	MS		LC	U	ñ	LL.	Ŧ	۵
	•	6	19.6	19.7	80.0	1.0	•			10.5	4 n
		•	•	•	•	•	•	•	•	•	•
+ 1	•	•	> <	•	•	•	•	•	•	●.	•
		10.4	> -	9 (• •	• •	• •			9. 0	
	• •			•	•	•	-		•	, .	•
22	11.9		22.1								11.7
54	-		2	23.2							
56		•	3.								14.
28 30	13.4	11.2	23.7	24°6 25°4	6.5	0 ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° °		m m 6 6	3°6 4°0	14.4 15.0	15.
32	14.7	11.7	25.1	26.3	1 .	1 .	3.6	1 .			16
76	•	-						4.6		16.4	20.8
36	•		9	28.3							2
38		12.4	7.								4
0.4		•	8		12.1	•	•	• [6.7	•	9
42	6	13.0		32.2			•				
77	20.5	13,3	30.9				•	•	•	- (_ (
	2				9	•	•	•	÷ (ů,	
30 (37 I	ى د	.		3/8	•	•	•	•	•	\$ v	c
50	5	14.4	36.0	. 1	20 · B	•	• 1	• 1	- 1	0 1	7 i
52		14.8		3	6					· 00	0
54		2	1.	46.8	0.70	•			ហ	· .	9
56	35.5		9 (•			~ (s o	0 1
60	48°5	17.2	56.3	65.7	45.0	n 00	7 œ	0.6	25.0	46.5	61.
	0	8 1	67.1		57.8			0	2	7.	00
			8	104.7	A3.1	•	10.3	10.0	•94	78	78.
99	187.8	21.1	174.4	- a - i	196.5	11.7	-	0	103.5	•	
	ROAD DIMEN	SIONS FOR		MANAGEMENT		ROAD	DIMENSION	S FOR SLO	PE S	AND END A	REAS
<u> </u>	DE WH	(6)	SF = SLOPE SC = SLOPE WH = TOT.	33	3 S S S S S S S S S S S S S S S S S S S	-		SC STA	SLOP SLOP CUT HOR.	01 01 16 16 15	00 -
1	HOADE SE	Ţ	F = LENG C = LENG	00	-0PE	STAKE	1	GRADE DAYLIGHT STAKF	= FILL = HOR.		STAKE

ROAD GEOMETRY DATA USING A 1.5 TO 1 FILL SLOPE

i	19.7	WS 19.8		1.0	C 1 0	01 •	F 0	HF 10.5	< 1 •
	0.	20.3	2.2	1.2	1.2		1.2		6.5
		20.7	2.6	1.5	1.4		2.5	11.2	
	0 (21.8	3.6) (6-		•	0. 0	• 4
	21.9	22.4		2.2	2.1	9.5	2.3	•	
1		23.0	4.7				•	12,9	
	23.0	23.7	5.3						13,3
		54.4	5.9				•	•	4.
	24.3	25.2	9°9 1°4	3.5	3.1	8.6	3. /	14.5	16.3
i	25.7	27.0	8.2						1 6
	26.5	28.0							_
		20.62	10.1			0		7	٠ س
	28°4 29°5	30.4	11.1	5.1	5.0	10.2	•	0. 0	25.4
i	30.7	33,3	13.7	5,5		10.3			1 :
	32.1	35.1	15.2			0	8 5		2
						10.5		23,1	35.2
	35.5					0	•		œ
	37.5	42.0	71.4			10.7	11.9		- 1
	40.1		24.3		•	10.8	13.5	. 6.	N, C
	43.I	0 0 0			D	0.11	0 6	, r	•
		60.2	20.00	0 (11.2	-		0
	59.3	69.2			7.6	11.4		47.9	9
	70.8			0	0		3	6	4
	93.2		87.0	11.8	11.4	11.9	48	81.	AS.
	194.5	221.1		3	Ni	• 1	8	2.	5
	WATERSHED M	MANAGEMENT	.	ROAD	DIMENSIONS	FOR SL	E STAKIN	D END A	EA
SF	= SLOPE = SLOPE = TOT•	015T. TO 01ST. TO 10TH DIST	0 TOE FILL 0 TOP CUT STURB. HOR. STURB. SLOPE	FILL	S THE STATE OF THE	SC STAKE	SF = SLOPE SC = SLOPE C = CUT H HC = HOR.	DI DI EIG DIS	TOE FILL TOP CUT
		OF FILL	SLOPF SLOPE	-\-		GRADE DAYLIGHT	11 11		STAKE TO

						,				SCOPE = . SC	
SLOPE PERCENT	SF	SC	3	S Js		L C	ပ	HC		<u>+</u>	A
10		10.2				•	•	9.5	1.0	10.5	
77	•	•	•	•		•	•	•	•	•	•
	•		•	• -	•	•		•	•	•.	•
	•	•	40	• (•	•	•	•	•	•	•
20	11.8	11.2	5	36	• •	2.5	2.2	• •		•. •	
	1 .	11.5	1 6	3,	1 .	1 .		1 .		1 . •	
	•	00	, (4	•				•	•	•
	•	• •	4	3	2					•	
		ì	S	9	•		•	•		4	
30			26.1	1	7.5	4.1	3.6	10.8	4.2	15,3	18.8
32	15.3	13.0	7 .	000				11.0		9	
34			7	6	6.6		•			9	2
36		13.8	0	0				11,3	ສຸຄ		4
38	80		0	2						ထ	~
	O.		-	8	12.8	6.1	•	-	7.1		6
42	20.4		1 2	5	14.3	9.9	5.9	1 .	1 4	10	1 8
77	1.	5	4	7.						2	S
46					17.8				6.6	. e	
48	5.			2				12.6		S	45.1
20	28.0	•	0	2°					12.5	27.8	9
52		18.2	43.6	6							0
54		6	7	3	σ	_			9	3	
26			-		34.4			13.9		7	
58	45.3	•	57.4	9	1.	11.8	0		5	٠ ص	68.1
60		22.2	65.6	9		12.8		14.7	27.9		9
			1	92.					9	3,	87.
49	9			3	. 46				55.	87.	01
99	218,3		90	47.	216.8	17.8			0	6	00
	D DIMEN	SIONS FOR	A	NAGEM	ŀ	ROAD	DIMENSION	S FOR SL	OPE STAKING	END A	REAS
1	DE WH LIGHT KE	1 (3)	SF = SLOPE SC = SLOPE WH = TOT • W WS = TOT • W LF = LENGTH	DIST. TO DIST. TO IDTH DIS IDTH DIS	TOE FILL TOP CUT TURB. HOR. TURB. SLOPE SLOPE	L		SC STAKE	11 11 11 11 11	DIST. TO DIST. TO EIGHT DIST. CUT	1 H S
1	SF_WS	\	C = LEN C = CUT	OF CUT	0	1	- Sr - ∓ 	DAYLIGHT STAKE	85 86	DIST	STAKE T
			0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	- I I	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		000000000000000000000000000000000000000		0 0 0

ROAD GEOWETRY DATA USING A 1.5 TO 1 FILL SLOPE

						3			0	o, o						- !									0 -			40			FILL CUT (E TO CL.
5 TO 1	A				6	11.		14.		17.			24.	26.	0 (32.		38.	45.	46.	51.	57.	63.	71.	80.		0.5	126.	9 1 0	0 1	TOP STAK STAK
SLOPE = .75	불	10,5	. 1	B. 0			. •.		14.1		. 1			-		• ! 0		å	4	•	8	•	S.	۰. ه	45. 9. 1.	:	œ i	97.0	Z13.6	L END	DIST. TO DIST. TO EIGHT DIST. CU HEIGHT DIST. FII
CUT S	L.	1.0	9 (•			∞				0.9		. 1		6	0		3.	5	7.	0	24°0	•	6	S	136.4	L STAN	SF = SLOPE C = CUT H HC = HOR. F = FILL HF = HOR. A = END A
	£	•	•		0		0	11.2		11.7	. 1	2	5		. ه		3.		4.		5.	9	7	7	18.6	: 1	0	22.2	***	S FUR SL	SC STAKE SC STAKE GRADE DAYLIGHT STAKE
	ပ	1.0	. (ه م م				5.1							• (•		-	2	•	5.	17.6	8.02	DIMEN	ROAD FILL TO THE SE
	רכ	1.3	• (2.2				6		\$ \$ \$	•			4.9	7.0		8.2		6	0		12.3		4		11.0	6	22.1	0.0	KOAL	+4+
	LF	1.8	• (4.8			6.9	. 1	8.6						9		-	(C)	27.3	31.6		4.44	74.7	71.	105.7	245		O TOE FILL O TOP CUT STURB. HOR. STURB. SLOPE L SLOPE SLOPE
	S.M	20.4	0 (22.2		23.7	24.5				0°82	6		32.7			8	40.6		46.4		54.3				0.00	10	141.5	C82.5	MANAGEMENT	151. T 151. T 1014 DI 1014 DI 0F FIL 0F CUT
	Ī	20.3				23.2	24.0				21.4	28.4			32.1		5	37.2				48.1	52.3			7.4/	.68	119.2	238.3	WAIENSHED	= SLOP = SLOP = TOI. = LENG = LENG
9 FEET	SC	10.4			•	11.8	12.1			9	13.6	14.1	14.6	15.1	N.	16.3		17.7	- ∞	19.4	0	21.4	2	. 4	25.5	: 1		32.7	8.78	NOTONO FOR	
WIDTH = 1	SF	10.0	•		•	11.9	12.4	•		\$.	14.9	15.7		7.	18.7	19.9	1.	55.9		27.0	6		•	42.1	9	• 1	75.	108.8	7.7.42	KOAU DIMEN	GRADE WH DAYLIGHT STAKE LLF FILL SF
AD	N N	10		91		50			26	80 c	30			36	38	0.5		77	46	849	20				28			49			

	WIDTH = 18	FEET							CUT	SLOPE = 1.0	TO 1
SLOPE PERCENT	SF	SC	13	S	T.	C	U	£	L	生	٧
	10.1	10.6	20.6	20.7	1.8	1.5		10.1	1.0	10.9	5.0
14	10.8	•	21.8			• •					
	11.2	•	22.5						•		•
8 C	11.7	11.9	23°2		•	•	0 0 1 0	11.1	- S - C		•
	16.4	• 1	0.12	• !	• [• 1	• 1		• 1	• 1	• 1
22	12.7			10				11.7		13.1	
54				9							
92					•		•	•	•		9
30	15.4	14.8	28.9	30.1	8.0	0.0	4°8	13.2	7 4 . 4	15.6	21.0
32	1 0	15.4	30.1	1 0	8.9	1 .	1 .			1 9	1 8
34	7.	9	- 6						- 4	7	S
36	8	9			1101	8 0	5.7	14.7	6.2	00	8
38	6		34.6		12.5					6	-
40	0	•		6	13.9					. 0	5
42	22.4	16	8	41.8	15.6		7.5	16.5		22.0	38.9
77	24.2	•	40°8		-	11.6		7		3	3
949	9	21.6	٠ س		6					ទ ស	7.
84	20	ů.	9		Š		6	œ	•	-	6
50	31.8	24.4	0 1		25.6	2		6		0 1	0 1
55	35.4	9	54.5			7	2.	Ι.	9	3,	9
54	40.1	7.	6		e 4	8	3	2	6	°.	S.
90	46.1	30.1	91	76.2		0	4.	ش	01	2	
		35.9	87.6		49.1 61.4	26.1	18.5	27.5	34.1		113.8
62	85.8	39.9	106.8	25.	81.5		1:	10	1 5	9	35.
49	5.		4	_	22		24.5	33.5	67.7	10	168.5
99	594.4	. 4	91.	°64	292.4	2	0	39.5	162.	52.	34.
8 0 0 0 0 0 0 0	ROAD DIMEN	SIONS FOR	WATERSHED	MANAGEMENT	1		DIMENSION	S FOR SLO	E STA	AND END AR	i iii
1	RADE WHADE WHADE		SF = SLOPE SC = SLOPE WH = TOT. WS = TOT.	DIST. T DIST. T WIDTH DI WIDTH DI H OF FIL	O TOE FILL O TOP CUT STURB. HOR. STURB. SLOPE L SLOPE	+ L→	II ONO	STAKE		DIST, TO DIST, TO EIGHT DIST, CUT	TOE FILL TOP CUT
111	SM		H H	H OF CUT EIGHT	<u>a</u>	1	\	DAYLIGHT STAKE →-HC→	H H	DIS REA	. STAKE TO CL - SQ. FT.
							8 8 8				

ROAD GEOMETRY DATA USING A 1.5 TO 1 FILL SLOPE

SLOPE	SF	၁၄	3	SA		ΓC	U	Ĥ		L I	⋖
i — .	,	11.1	21.2		1.8			10.7	1.0	10,5	5.2
71		C•11	6	ů	•		† †	• .			
14	•	12.5	8.77	9 3		•		- 6	•		•
0 0	• ~	•	•	· L	•	•	•	1 0		ο	•
		•	25.7	26.2			2.7	3.6	•	12.7	•
22	13.2	14.3		27.5						13,3	
54	3							4	•		
56	. 4	15.9	56.62					5			8
28	15.5		31.0	32.2	7.5	80°C	4 i		7°4	15,3	21.2
30		17.8	32.7		•	• (9 1		οi	9
32	17.4	8	34.6		9.6			7.			7.
34				38.8		11.7	6.5		0 • 9	$\boldsymbol{\omega}$	
36	20.0	21.6		1.				0			. 4
38	1.	3.			•			-			8
0 7	3°	5.	45.0				•	3	•	2	3.
42	5.	i ~	48.6	52.8	17.7				•	3	6
77	27.75			7	C	21.8		_	11.2	25,8	
9+	0	33.3						6		φ. Φ	5.
	4.	7.		71.3		8	16.1	،		•	2
50	80	41.9	72.0	80.5	31.1	3		7.	• 1	•	7
		48.0	1.	2	6.		2	8	0	6	3,
		26.0	• 46	7.	4	8	9	œ	. 4		N.
26		7.	12.	or .		6	8	œ ,	0	\$	53
50 60	100.7	109.2	138.5	100.1	4 4 60 4 4 60	101.3	56.2	93.3	51.8	86°4	263.1
	145.1	157.4	57.	1 2	37.	164	16	33.	1 9	23.	88
64		•	450.0	34	64	70		33.	38.	16.	01.
99	34	5	00				18.	_	69	863.8	4
1 1 1 6 5	AD DIMEN	SIONS FOR	MATERSHED	MANAGEMENT	1	ROAD	DIMENSION	L 1	PE STAKI	END A	REA
<u> </u>	WH OE IGHT	137	SF = SLOPE SC = SLOPE WH = TOT	DIST. T DIST. T WIDTH DI	TOE FILL TOP CUT	i .		SC STAKE	SF = SLOPE SC = SLOPE C = CUT H	DIST. DIST.	TOE FI TOP CU
-1	RONO SFILL SES	1		IDIH DI OF FIL OF CUT	В. ОРЕ ОРЕ	STAKE F	ROAD FILL SEAS	GRADE	11 11 11	DIST. CUT HEIGHT DIST. FILL	STAKE 1

10 10 10 20 20 20 20 10 1	10 10 10 10 10 10 10 10	- :	WIDTH = 19	FEET							cut s	SLOPE = VER	TICAL
10.6 10.4 20.5 22.5 23.6 1.9 1.0 1.0 0.5 1.1 1.0 0.5 1.0 1.0 0.5 1.0 1.0 0.5 1.0 1.0 0.5 1.0 1.0 0.5 1.0 1.0 0.5 1.0 1.0 0.5 1.0 1.0 0.5 1.0 1.0 0.5 1.0 0.5 1.0 0.5 1.0 0.5 1.0 0.5 1.0 0.5 1.0 0.5 1.0 0.5 0.5 1.0 0.5	10.0 10.4 20.5 20.6 2.9 1.0 1.0 0.5 1.0 11.0 0.5 1.0 10.5 20.5 20.6 2.9 1.5 11.5 11.6 0.5 20.5 20.5 20.5 20.5 1.5 11.5 10.5 20.5	SLOPE PERCENT						LC	U		L .	¥	A
10.0 10.5 10.5 21.5 21.5 22.5 3.7 15.5 1	10.5 10.5 21.3 21.5 21.5 21.5 15.5		•	•	0	0 -		1.0	1.0		0.1	0.	
12.5 11.2 22.5	11.7 10.7 21.7 21.9 3.2 1.7 1.7 1.7 1.9	71	•	•	• -	• -	•	1	-		•	•	•
11.7 10.8 22.5 22.5 3.7 1.9 1.9 9.5 2.4 13.6 11.2 12.5 11.1 23.0 23.6 4.8 2.4 2.4 9.5 2.4 13.6 11.2 13.6 11.2 23.5 23.5 24.2 5.5 2.4 2.4 9.5 2.4 13.6 11.2 14.6 11.8 24.7 24.7 24.8 2.4 3.1	11.7 10.8 22.5 22.5 3.7 1.9 1.9 5.5 2.4 13.6 11.2 12.6 11.1 23.0 23.6 4.8 2.4 2.4 2.4 3.7 3.1	16	11.3	•	• -			1.7					• •
12.1 10.9 22.5 23.0 4.3 2.1 2.1 9.5 2.4 13.0 11.5 13.5 11.2 23.5 24.2 5.5 5.6 2.4 3.1 3.1 3.1 14.0 14.6 11.8 25.3 25.6 6.8 3.1 3.1 3.1 9.5 3.6 14.0 14.6 11.8 25.3 26.4 7.6 3.4 3.7 3.1 9.5 3.6 14.6 11.8 25.3 26.4 7.6 3.4 3.7 3.1 9.5 3.6 15.3 12.0 26.8 28.3 3.1 3.1 3.1 3.1 3.1 3.1 16.1 12.2 26.8 28.3 3.1 3.1 3.1 3.1 3.1 17.8 12.7 26.8 28.3 3.1 3.1 3.1 3.1 18.8 12.7 26.8 28.3 3.1 3.1 3.1 3.1 3.1 18.8 12.7 29.5 31.6 33.2 11.4 4.5 4.8 9.5 5.7 18.8 12.7 29.5 31.9 31.8 15.6 5.1 5.1 3.1 22.3 13.5 31.6 33.3 3.1 3.1 3.1 3.1 24.7 14.2 35.0 31.8 19.3 6.1 6.5 6.5 6.5 9.5 26.8 14.5 37.0 41.4 21.6 6.5 6.5 9.5 12.0 27.8 26.8 17.8 19.0 90.0 10.0 26.8 17.8 19.0 90.0 10.0 26.8 17.8 19.0 90.0 10.0 26.8 17.8 19.0 90.0 26.8 17.8 19.0 90.0 26.8 10.7 8.8 8.8 9.5 12.0 27.1 27.2 10.5 10.0 28.8 19.0 90.0 10.0 28.8 10.0 90.0 10.0 28.8 10.0 10.0 28	12.5 11.1 23.0 23.6 4.8 2.4 2.4 2.4 3.5 11.2 13.5 11.2 13.5 11.4 23.0 23.5 24.6 2.4	18	11.7	•	2.	2			•				
12.5 11.1 23.0 23.5 54.2 5.6 2.6	12.5 11.1 23.5 24.2 4.4 2.4	20	12.1		2.	6)	•	•			• [•	•
13.0 11.2 23.5 24.2 5.5 2.6 2.6 9.5 3.4 14.0 14.3 14.0 11.6 24.7 25.6 6.8 3.4	13.5 11.2 24.4 24.2 24.2 2.6 2.6 2.6 3.4 14.6 14.3 14.3 11.6 24.1 24.4 2.6 2.6 3.4 3.4 3.4 3.4 3.5 3.4 14.6 14.3 14.3 14.5 11.6 24.1 24.4 2.6 3.4 3.4 3.4 3.4 3.4 3.5 3.6 14.5 17.4 14.5 11.6 24.7 25.6 27.3 25.4 3.7 3.	22				3.							
13.5 11.4 24.1 24.9 6.1 2.9 9.5 3.4 14.6 15.9 17.6 15.9 17.6	13.5 11.4 78.1 24.9 6.1 3.9 3.1 3.4 14.6 15.9	24				4.					•		
14.6 11.6 25.3 25.4 7.8 3.1 3.1 9.5 3.8 15.2 17.4 16.1 12.2 26.8 27.3 8.4 3.7 3.7 3.4 9.5 4.7 16.5 20.8 16.1 12.2 26.8 28.3 9.3 3.9 3.9 9.5 5.7 16.5 20.8 16.1 12.2 26.8 28.3 9.3 10.3 4.5 4.5 9.5 9.5 7.0 20.0 17.8 12.7 28.5 30.5 11.4 4.5 4.5 9.5 9.5 7.0 20.0 18.8 12.9 29.5 31.9 34.8 12.6 5.4 9.5 9.5 17.0 22.9 13.5 31.9 34.8 17.2 5.8 5.4 9.5 12.0 20.0 22.9 13.8 13.9 34.3 24.4 2.16 6.5 6.5 9.5 10.7 20.0 22.9 13.8 13.9 34.8 17.2 5.8 9.5 10.7 20.0 22.9 13.8 13.9 34.8 24.4 2.16 6.5 6.5 9.5 10.7 20.0 22.9 13.8 13.9 34.8 2.4 6.5 6.5 9.5 10.7 20.0 22.9 13.9 34.8 2.4 2.16 6.5 6.5 9.5 10.7 20.0 22.9 13.9 34.8 2.4 2.16 6.5 6.5 9.5 10.7 20.0 22.9 13.9 34.8 2.4 2.16 6.5 6.5 9.5 10.7 20.0 22.9 15.0 20.0 20.0 20.0 20.0 22.0 17.2 5.6 39.1 20.0 20.0 22.0 17.2 5.6 39.1 20.0 20.0 22.0 17.2 5.6 39.1 20.0 20.0 22.0 17.2 5.6 39.1 20.0 20.0 22.0 17.0 20.0 20.0 20.0 22.0 17.0 20.0 20.0 20.0 22.0 17.0 20.0 20.0 20.0 22.0 10.0 20.0 20.0 20.0 22.0 10.0 20.0 20.0 20.0 22.0 10.0 20.0 20.0 20.0 22.0 10.0 20.0 20.0 20.0 22.0 10.0 20.0 20.0 20.0 22.0 10.0 20.0 20.0 20.0 22.0 10.0 20.0 20.0 20.0 22.0 10.0 20.0 20.0 20.0 22.0 10.0 20.0 20.0 20.0 22.0 20.0 20.0 20.0 20.0 22.0 20.0 20.0 20.0 20.0 22.0 20.0 20.0 20.0 20.0 22.0 20.0 20.0 20.0 20.0 22.0 20.0 20.0 20.0 20.0 22.0 20.0 20.0 20.0 20.0 22.0 20.0 20.0 20.0 20.0 22.0 20.0 20.0 20.0 20.0 22.0 20.0 20.0 20.0 20.0 22.0 20.0 20.0 20.0 20.0 22.0	14.6 11.8 72.7 75.5 76.8 3.4 3.4 3.4 3.5 3.4 3.5 3.4 3.5 3.4 3.5 3.4 3.5 3.4 3.5 3.4 3.5	56				41					•		
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ROAD GEOMETRY DATA USING A 1.5 TO 1 FILL SLOPE

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ROAD GEOMETRY DATA USING A 1.5 TO 1 FILL SLOPE

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DIMENSIONS FOR MATERSHED MANAGEMENT ROAD DIMENSIONS FOR SLOPE STAKING AND END AREA SC = SLOPE DIST, TO TOP CUT SC = SLOPE DIST, TO TOP WH = TOT. WIDTH DISTURB, SLOPE STAKE F MONOR		61.	36°	51.	01.	59	7.	2.	. 9	• 44	225.	94.
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+ OH + H - H - H - H - H - H - H - H - H -	1			= CUT	IGHT		1		STAKE	LAND	DEA OF CH	1

ROAD GEOMETRY DATA USING A 1.5 TO 1 FILL SLOPE

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AD DIM	ENS 10	ATFRSHE	I Z		1 4	i 🚍	IS FOR SLO	PE STAKIN	D END A	
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STAKE STAKE TO FILL TO		OT.	O I A I	URB. URB. SLOPE	FILL F RG	ROAD FILL TO SECOND	GRADE	C = CUT + HC = HOR. F = FILL.	EIGHT DIST. CU HEIGHT	STAKE
SFWS		C = LENG C = CUT	H OF CU EIGHT	-0 T	1	ñ 5	DAYLIGHT	= HOR.	⊢ ₩	STAKE

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	L.	1.1	E .			2.0							6.3			• 1			13.5		•	21.5	J.	31.9	40°7 54°7	10	45	0.1	E STAKIN	SF = SLOPE SC = SLOPE C = CUT H HC = HOR. F = FILL HF = HOR.
	HC	11.2			•	13.7	14.4		15.8			9	19.8	- (22.6	•		8	31.5	. 47	6	4	Ϊ.	-	75.7 98.5	40.	46	98	S FOR SLOP	SC STAKE SC STAKE GRADE DAYLIGHT
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	٦٦	•			•	2.1			7.6		1.6	11.0	12.4	13.9		. 1	20.2	3	56.4	° C	35.6		20.7	62.4	79.5 106.9	1 5		1176.2	ROAN	FILL
	اما ا	1.9	4.0		J.J.	7.04	5.4	6.2	C -			10.1	11.4	ᢤ,	•	١٥	φ •	Ļ	° 7	ď	32.9	8	9	7	73°3 98°6	45.	62.	4	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	TOE FILL TOP CUT URB. HOR. URB. SLOPE SLOPE SLOPE
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	SC	•	12.1		ຳຕ	14.4	i •		9	17.7	8	0	21.3	٠ . ز	• † v	٥١	0.65	•	35.1	6	4 .	0	6	70.A			93	4	SIONS F	
	SF	10.8	•	1. 2. c.		13.3	13.9				17.3	18.4	19.6	• (75.20	•		6	2	9	40.8	9	54.5	2	81.0		70.	092	OAD DI	GRADE WH GRADE DAYLIGHT STAKE NOAD TENTERS ROAD TENTERS ROAD TENTERS
1	SLOPE	-	2			20			26		30		34						46						58 60			99	1 1 1 2 2 1 1	

ROAD GEOMETRY DATA USING A 1.5 TO 1 FILL SLOPE

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11 12 13 13 14 14	10.9	21.6	-		1.1		10.0	1 . 1	11.6	5.8
11. 12. 13. 13. 14. 15.	11.0	2	S							
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13.	11.7					2.5	0		4.	4
14.	11.8	4	5	5.7			10.0			15.9
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22	_	8	9		5.7		10.0	0.6	6	
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2	21.9	187	224		12.1	12.1	10.0	-	177.1	110.7
AD DIM	NSIONS F	ATERSHE	ANAGEM	İ	ROAD	DIMENSION	S FOR SLO	PE STAKIN	AND END AR	i lui
	; ! ! ! ! ! !	F = SL0	DIST.	TOE FILE	i		CUT	! ! !!	0151. 10	T0E
GRADE DAYLIGHT	1205	07S = 0	DIST. TO	С			SCA	= SLOP	DIST	OP C
STAKE		W = TOT = W W S = TOT = W	IOTH OIS IOTH OIS	മെ	-	FILL TOTAL	A 1 PC	HC = HOR.	EIG	STAKE TO
ROADERS	Ţ.	11 1	OF FILL	900	STAKE RO	1	GRADE	11 1	EIGHT	CIAK
CM			IGHT	5	1		STAKE	1 11	REA OF	50.

ROAD WIDTH = 20 FEFT

CUT SLOPE = .10 TO 1

	SF	SC	I	SM	L.F.	٦٥	U	HC	L£.	L I	٧
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		11.2	2	8		•			•	0	
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		11.5	2.4° 0.4°	24.5	4.5	2.3	0 m % % % % % % % % % % % % % % % % % %		• •	13. 13. 13.	
22	1 .	11.9	1 4	5 1		1 .					
54			2	2	5.8					14.8	
26		2	2	9							7
X 00 00 00 00	15.6		26.4	- &						16.0	19.7
32	16.3	1 .	27.8	29.5	6.8		1 .			17.4	10
34				c				0		80	5
36	œ :	3.		1.						6	7 .
38	19.0	13.8	30.6	° 4	~. ~. ~. ⊓			10 0.0	1.0° L	20.1	
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1 U	7 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	15.5	x • • • • • • • • • • • • • • • • • • •	41.9	0° c c c	0 n	7 - 7	100	11.4	20.3	4 a
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			45.6	00				10.8	14.5	0.	
	S	7 •	S	Ĉ	0				9	4	
	6	7		-	• 4				6	ο. Φ	o.
60 60	45°4 53°9	18,3	55.1 62.6	63.7	41°0	N 6 6		10.9	22.8	44.1 51.6	68.3 75.5
		ic	1 :		1 3	7 0 6	7 01		1 4	10	1 3
	، کا -	° -	0.00	. v		0 1		-	5.12	9 9	9
99	208	(m)	193.	232	1 1	13.0	12.9	11.3	S.	182.4	117.8
† † † † †	AD DIM	STONS F	ATERSHED	MANAGFME	\$ 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	I	=	S FOR SLO	STAKIN	AND END AR	FAS
	GRADE WH DAYLIGHT STAKE	07/	= SLO = SLO = TOT	DIST. TO DIST. TO WIDTH DIS	E FILL P CUT B. HOR.	-		SC STAKE	SC	DIST, TO DIST, TO EIGHT	TOE FILL
	ROADER SE		LF = LENGT C = CUT H	WIDIH DIS H OF FILL H OF CUT EIGHT	• • • • • • • • • • • • • • • • • • •	STAKE	ROADFILE	GRADE DAYLIGHT STAKE	F = FILL HF = HOR. A = END A	DIST. FILL DIST. FILL REA OF CUT	STAKE TO C. STAKE TO SO. FT.

ROAN GFOMETRY DATA USING A 1.5 TO 1 FILL SLOPE.

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SLOPE ERCENT	SF	SC	T A	S	L.	٦٦	U	HC	 La. 1	L.	∢
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		11.2	2	2							
		11.4	8	~			•				œ
	12.0	11.6	3	3							
			3	4 .					•		-
	12.9	12.0	4 .	. 4			2.4		2.5		3
22	13.4			5				10.7			4.
	13.9		5	9							
		12.7	9	7.	6.6						8
	15.1	2.	7.	Œ						16,1	0
	15.8		7 。	0.62		3.9	3.8	10.9	•		5.
32	16.5	13.5	1 00	0	9.1			11.0		7.	4
	7	3	6							8	9
	80	4	0	2°			0			6	æ
	19,3	4.	_	3	12.4			11,3		20.3	
	0		5	5				11.4	•	-	4 •
	1 -	1 .	34.1	7.	5.			11.5	8.4	22,7	7.
	3		2	6	8					. •	0
	5.	16.1	7.	41.2						2	
	_		6	3,	21.1			11.8		7.	7.
	6			9	3.	7.9	7.7	•	•	6	51.3
5.2	iN	- 2	1 4	0		•		•	5	2 .	5
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	6	3,	103.6	23	96	13,1			3.		
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	GRADE DAYLIG STAKE		l .	DIST. TO DIST. TO WIST. TO	E FILL P CUT B. HOR	i i		35	1 11 11 11	DIST. TO DIST. TELEGHT	TOE FIL TOP CUT
	ROAD THE SE		S = 101 C = LFN	WIDTH DISH OF FILL	TURB. SLOPE SLOPF SLOPE	FILL	ROAD FILL SEASON	GRADE DAYLIGHT STAKE	= HOR. = FILL = HOR.	DIST. HEIGH DIST.	STAKE T
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SLOPE ERCENT	14 S	SC	3	SA	 	rc	S	HC	 	¥	A
==	11.0	11.3	22.2	22.3				10.6		11.6	6.0
	11.7	11.7	س	ا	•	•	• •		•). C	•
	12.2		3°	4.			•				•
18	12.6		4 1	4 N	•		2°0	11.1		0.	
	1001	• 1	·i	•	•	• 1	• 1	• 1	• [• [e [
	•	•	5	9	•			11.4			
	•	13.1	9	7.			•	11.5	•		
	•	13.4	•	x (•	•	ô,
3Ú 3Ú	16.2	13.7	• •	30.3	. a.	4 ° 1	4.1	12.0	4 4	17.0	
	7.	14.5		-	0°0						1 %
	17.9		-	32.8		5.4	4.8	12.4	5.8	8	
	е Ф (15.3	2	41	11.5				•		0
	°,		m,	° 1	8 2		•	•	•	°,	۳,
	- 1	. 1	9 1	- 1	. (•		• 1	- 1	9
	2		6.	6	15.8					23,2	0
	4.		80		7					4.	3
	9		40.5					.	11.0		47.6
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52	4	20.3	8	4	28.5				5	3	2
	ဆ	-	2.	6	~		10.1		œ	2	œ
	e e	25.2	57.2	20				15.4	21.2		2
	0	9	3.	3.	ີ				S		
60		24.7	72.9	85.0	2	• [12.7	16.4	; ;	9 1	40
	76.	6.		02.	72.5		13.9		0	. 0	7
64	108.5	28.5	•	137.0			15.4	17.7	58	0	125.7
	42.	2		74.	4	•	17.7		.	0	
	D DIMEN	SIONS FOR	ATERSHI	MANAGEMENT			DIME	S FOR SLO	PE STAKIN	D END A	EAS
	SRADE WHOSTALIGHT	1 37	= SLO = SLO = TOT	DIST. TO DIST. TO WIDTH DIS	OE FILL OP CUT RB. HOR.	i		SC STAKE	1	DIST, TO DIST, TO EIGHT	OE FI
	ROAD FILL AS A THE ROAD TO SE WS	1		WIDTH DIS H OF FILL H OF CUT EIGHT	RB. SLO LOPE LOPE	STAKE	ROAD FILL TO A	GRADE DAYLIGHT STAKE	HC = HOR. F = FILL HF = HOR.	DIS HEI DIS RFA	STAKE T STAKE
1								-	1		200

ROAD GEOMETRY DATA USING A 1.5 TO 1 FILL SLOPE

	SF	28		SM	ls.	LC	O	HC	ls.	Ŧ	۵
10	11.1	11.5	22.5	22.6	0.0	1 4 . [1.1	10.9	1.1	11.7	6.1
	11.9	12.1	m	4				11.3	1.6	12.5	
	12,3	12.4	4 .	. 4				11.5	1.9	12.9	
	12.8	12.7		2				11.7	2.3	13.4	
	13,3	13.1		9	4.7	0 1	• [11.9	•		4 .
	3		9	7.				12.2			
			51.5	8				12.4	•	15.0	7
	° .	14.2	8	29.3	6.8				•		6
30	15.8	14.7	• •	0	7.7	0°0°0°0°0°0°0°0°0°0°0°0°0°0°0°0°0°0°0°	0 7 7	13.0	• •	16.4	22.1
	17.5	15.7	1 0	1 .						1.00	7.
			32°8	34.7		6.5	5.2		5.9	18,9	6°62
	6				11.9					6	00
	· ·	17.4						14.6		-	9
	22.1	. 1	37.4	. 1	14.8	0			• 1	2	o i
	3.	18.9		8				15.5		6	6
	S.	.6		5	000			5.		S	7 .
46	27.6	20.6	43.7	48.1	8000	10.7	9 00	16.4	11.5		
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50	2:	è i	6 1	2		• 1	0	7.	• 1	2	9
	9		3			13.7			. 9	5	0
	-	25.1	φ.	9				6	6	6	φ. ι
	•	26.6	\$,	ر س (41.2			6	21	\$ -	•
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ROAD GEOMETRY DATA USING A 1.5 TO 1 FILL SLOPE

Megahan, Walter F.

property for low-standard roads for watershed management considerations, slope staking, and end areas. USDA For. Serv. Gen. Tech. Rep. INT-32, 104 p. Intermountain Forest and Range Experiment Station, Ogden, Utah 84401.

Tables provide various dimensions for low-standard roads built with a "balanced" construction technique. In addition to assisting in slope staking and in the determination of excavation volumes, the information offers a means of evaluating potential watershed impacts of road construction and aids in the planning of appropriate erosion-control measures. The material is applicable to both the road location and design phases of road construction.

OXFORD: 116; 116.5; 116.65; 383; 686.3

KEYWORDS: watershed management, road erosion, road construction, road prism, road design, erosion control, sedimentation

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